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THESIS

USE OF THE TI 59 WITH APPLICATIONS TO
PROBABILITY AND STATISTICAL ANALYSIS

by

George Russell/Nelson

Edgar Emmett Stanton III

December 1980

Thesis Advisor:

P. W. Zehna

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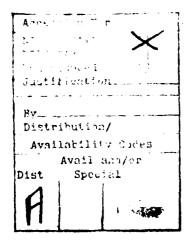
This thesis demonstrates through three comprehensive examples, the capabilities of the TI 59 programmable hand-held calculator as an analytical tool. One example is a probability application while the other two examples entail use of the TI 59 in statistical inference and data analysis. The probability example involves the use of the Monte Carlo technique to simulate stochastically the detection, identification and engagement of a cruise missile by an Improved Hawk Air Defense Battery.

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The second example illustrates a TI 59 program which is designed to analyze sample data. The data used for this illustration were gathered by the authors in an experiment which encompassed the testing of thirtysix male subjects to determine the extent to which their training routines influenced their strength, endurance, and cardiovascular fitness. The third example involves the use of an ANOVA routine and Scheffe's multiple contrasts to demonstrate how the TI 59 may be used to facilitate statistical inferences. The fitness data are also used for this purpose. The intent throughout the thesis is to exemplify the capabilities of the TI 59 as a viable, real world analytical tool rather than emphasize particular results of the simulation or the experiment.



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Use of the TI 59 with Applications to Probability and Statistical Analysis

by

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Submitted in partial fulfillment of the requirements for the degree of

MASTER OF SCIENCE IN MANAGEMENT

from the

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NAVAL POSTGRADUATE SCHOOL December 1980 D Approved by: Thesis Advisor Co-Advisor Chairman ment of Administrative Science wind

Dean of Information and Policy Sciences

#### ABSTRACT

This thesis demonstrates through three comprehensive examples, the capabilities of the TI 59 programmable hand-held calculator as an analytical tool. One example is a probability application while the other two examples entail use of the TI 59 in statistical inference and data analysis. The probability example involves the use of the Monte Carlo technique to simulate stochastically the detection, identification and engagement of a cruise missile by an Improved Hawk Air Defense Battery. The second example illustrates a TI 59 program which is designed to analyze sample data. The data used for this illustration were gathered by the authors in an experiment which encompassed the testing of thirty-six male subjects to determine the extent to which their training routines influenced their strength, endurance, and cardiovascular fitness. The third example involves the use of an ANOVA routine and Scheffe's multiple contrasts to demonstrate how the TI 59 may be used to facilitate statistical inferences. The fitness data are also used for this purpose. The intent throughout the thesis is to exemplify the capabilities of the TI 59 as a viable, real world analytical tool rather than emphasize particular results of the simulation or the experiment.

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this effort possible.

#### I. INTRODUCTION

The intent of this thesis is do demonstrate through three comprehensive examples, the tremendous capabilities of the TI 59 programmable hand-held calculator. One of the examples is a probability application while the other two entail use of the TI 59 in statistical inference and data analysis.

The example chosen to illustrate an application to probability theory is a combat simulation model. The model involves use of the Monte Carlo technique to simulate stochastically detection, identification, and engagement of a cruise missile by an Improved Hawk Air Defense Battery. Chapter III discusses the combat model and the TI 59 simulation in detail. Chapter II addresses briefly the Monte Carlo technique, combat modeling in general, and the TI 59 random number generator in order that the reader may better understand the combat model discussed in Chapter III.

Two examples are provided for statistical applications of the calculator. These involve the analysis of data gathered by the authors in a physical fitness experiment. The experiment, discussed in detail in Chapter IV, involved the testing of thirty-six male subjects who were divided into six categories based on their training routine, to determine whether the subjects' training program did in fact influence their physical fitness. Chapter IV describes the fitness experiment in terms of its scope, design and scoring methodology. Chapter IV also discusses a TI 59 program which computes measures of central tendency and spread and then illustrates the use of the program with the fitness data.

Chapter V describes a TI 59 program for analysis of variance and then demonstrates how the program may be used with fitness data to make statistical inferences.

Throughout the thesis, it is assumed that the reader is generally familiar with programming techniques for the TI 59 hand-held calculator. Subroutines, labels, flags, data registers, and program steps are discussed in each of the ensuing chapters where the intent is to illustrate how the features of the calculator may be exploited to facilitate statistical analysis or simulation. Reference 12 discusses programming techniques for the TI 59. The TI 59 has one particular feature which makes it much more than a calculator. Specifically the capacity to use subroutines provides a analytical tool more like a minicomputer than a calculator. The three programs discussed in the succeeding chapters use subroutines extensively to illustrate this powerful capability.

Finally, while a few of the referenced tables and charts of this thesis are positioned close to comments discussing their purpose, most are to be found at the conclusion of each chapter or in the appendices.

## II. PROBABILITY

The intention of the authors was to begin this chapter discussion with a definition of probability theory, that branch of mathematics generally believed to have been founded by a Swiss mathematician named Jacques Bernoulli. However, research has revealed that there is some discussion as to the true meaning of probability theory and that among mathematicians there appear to be those who view probability as a state of the universe while others consider probability a state of belief. To compound this situation furthermore, there appear to be differing definitions of probability within each group. Indeed, all attempts to define probability directly have failed to meet with success. Instead, probability has been axiomitized, much like geometry, so that a set of consistency rules or axioms established by A. Kolmogorov are now generally accepted by the scientific community. These axioms allow a great deal of freedom in the assignment of probabilities for any particular model and at the same time force any such assignment to be consistent with any other. Moreover, the theorems of that theory then become universally true statements for any such assignment. In this system, events are defined as sets in a specified sample space. With those guidelines as a background, probability theory can be used to make intelligent predictions and decisions if we know what events are possible and how probable are the various events. After a little thought it becomes immediately apparent that the immense power of such a tool as probability theory is limited in use only by one's imagination and

ingenuity. This research is all effort to use probability theory in the construction of a probabilistic combat simulation on the Texas Instruments programmable 59 calculator (TI 59). Because the simulation developed includes a number of the many chance elements involved in most combat situations, a discussion of the Monte Carlo technique and random number generation on the TI 59 follows. A brief disussion of combat model simulations concludes this chapter.

### A. MONTE CARLO TECHNIQUE

Systems that exhibit stochastic elements in their behavior can be simulated with the aid of the technique called Monte Carlo (named after the famous gambling resort town of Monaco). This technique involves sampling from those known probability distributions that represent each of the actual chance processes included in the system under study Ref. 9. By completing a system simulation run many times while keeping the non-stochastic inputs constant but allowing the chance elements to fluctuate according to their known probability distributions, a statistical average for run results can be determined.

Turban and Meredith Ref. 8 have listed the steps necessary in building a Monte Carlo simulation as follows:

- "1. Describe the system and obtain the probability distributions of the relevant probabilistic elements of the system.
- 2. Define the appropriate measure(s) of performance.
- Construct cumulative probability distributions for each of the stochastic elements.
- 4. Assign representative numbers in correspondence with the cumulative probability distributions.
- 5. Generate a random number for each of the independent stochastic elements and . . . (determine) the measure of system performance.
- Repeat step five until the measure of system performance stabilizes."

Thus the distinguishing feature of the Monte Carlo method is the repetitive execution of an established experiment or simulation involving
randomness.

While electronic digital computers themselves are not necessary for the execution of simulations, they do offer tremendous speed and consistency of conditions for such models. Thus the computer is ideally suited to perform the large number of repetitions required by Monte Carlo but the matter of landomness presents a problem. For the Monte Carlo technique described above the necessity of a truly random number is essential. However Kovach Ref. 6 notes that:

"Strictly speaking, the random number exists only as the result of a random process."

While computers, to include the TI 59, do possess the capacity to continuously generate random numbers as they are needed, these numbers are subject to the limitations of the computer and are not truly the result of a random process and hence are often described as pseudo-random.

### B. TI 59 RANDOM NUMBER GENERATOR

R.F. Barton Ref. 4 describes simulation as follows:

"Simulation is simply the dynamic execution or manipulation of a model of an object system for some purpose.

Simulation is a case-by-case method for studying object systems. Each case might be either a single trial or an entire run. In either view, outputs may differ trial to trial and run to run."

The object system is that system under study in the simulation.

The TI 59 in its capacity as an electronic computer provides the user with the means of developing and executing stochastic and nonstochastic simulations.

Barton continues [Ref. 4] :

" A stochastic simulation is one in which differing outputs trial to trial can be obtained without changing the inputs (ignoring random numbers as inputs). Specifically, this means that identical parameters, starting conditions, and input time path values produce varying outputs trial to trial and run to run.

A nonstochastic simulation is one in which the inputs or the model must be changed to obtain changed outputs. This means that identical model operations, parameters, starting conditions, and input time path values will produce identical outputs run to run. "

There are inputs common to both of these simulation types. However, as alluded to above, there are also special inputs that are needed to represent the chance processes or stochastic events found only within a stochastic simulation. These special inputs are random numbers.

The characteristic of random numbers that makes them different from all other numbers is the fact that the knowledge of any future random number cannot be enhanced by the knowledge of any past, present, or other future random number.

The TI 59 with its master library module solid state software program ML-15, a random number generator, can generate sequences of uniformly or normally distributed random numbers independent of a simulation program or within such a program.

Kovach states Ref. 6 :

"(Random) numbers generated by the computer are sometimescalled pseudo-random because they are subject to the limitations of the computer. In a list of truly random numbers, for example, one would expect to find numbers containing more digits than can be obtained in a computer."

Random numbers produced by the TI 59 ML-15 program are generated by a mathematical formula. Given an initial seed number by the user, this

program will always produce the same list of pseudo-random numbers. Thus if repeatedly initialized with the same seed number the forth-coming random numbers would be known and randomness would not exist. That is, every future random number could be predicted. Hence, the randomness of the numbers produced by the ML-15 program are as dependent upon the user as the mathematical formula of the program itself. It is therefore incumbent upon the routine user of the ML-15 program to vary the seed number used within denoted limits to insure genuine pseudo-random numbers.

The TI 59 ML-15 random number generator program is listed in Table 2-1. User instructions for the ML-15 program [Ref. 11] are listed in Table 2-2. Data register contents are listed in Table 2-3.

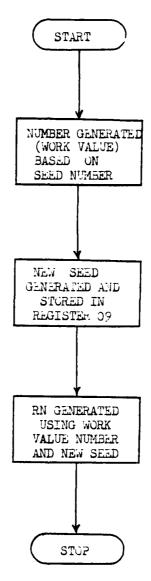
While the program does provide the option of generating uniform numbers for ranges other than 0-1 and also provides statistical data for the random numbers generated, only the generation of the uniform, range 0-1, and the normal random numbers will be discussed further.

### 1. Uniform Random Number Generator

A flowchart of the uniform random number generator, range 0-1, is displayed in figure 2-1. Program steps 000 through 054 contain the following mathematical formula, called the linear congruential method Ref. 11, for the generation of these numbers. (Throughout this thesis an asterisk is used to indicate multiplication.)

((24298 \* SEED + 99991) : 199017 STO 07)

A work value is the result of the above operation. This result remains in the display register. The value 199017 is stored in data register 07, an ML-15 work register.



TI 59 Uniform Random Number Generator FIGURE 2-1

Calculation continues.

(INV INT \* RCL 07) STO 09

The integer portion of the number resulting from the previous operation is discarded, then the remaining fractional portion is multiplied by 199017 which was stored in data register 07. This product then is stored in data register 09 and becomes the seed for the next random number calculation. Calculation continues.

((RCL 09 ÷ RCL 07) \* 5 INV 2nd log)

Now the new seed is divided by the number 199017 which was stored in data register 07 during the first operation. This quotient is then multiplied by the common antilogarithm of 5 to complete the step.

Calculation continues.

(INT ÷ 5 INV log)

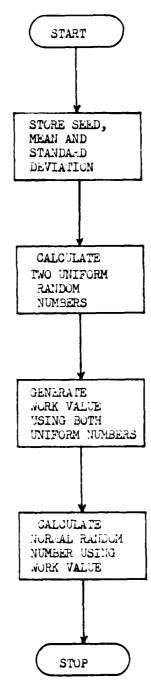
The fractional portion of the previous numerical operation is discarded and the result divided by the common antilogarithm of 5. This quotient is then displayed as the uniform random number, range 0-1.

## 2. Normal Random Number Generator

A flowchart of the normal random number generator is displayed in figure 2-2. Program steps 069 through 135 contain the following mathematical formula, called the direct method Ref. 11 for the generation of these numbers.

(seed STO 09)
(mean STO 10)
(standard deviation STO 11)

Following program initialization, three data values are entered and stored in data registers 09, 10, 11. The seed number, the desired normal distribution mean (mu) and the desired normal standard deviation



(sigma) are stored in these registers as listed respectively. The seed value is limited as noted in the TI user instructions, table 2-2.

(SBR DMS STO 08 SBR DMS)

Initially the program calls the previously discussed uniform random number generator to produce such a number and then stores it in data register 08. The uniform generator is called again to produce another uniform random number which remains in the display register for manipulation and is denoted RN. Calculation continues.

((RN \* 2 \* 17 ) COS) \* ((RCL 08 Lnx) \* (-2)

The uniform random number in the display is next multiplied by two pi.

The cosine of this product is then calculated. The resulting value is multiplied by the product of the natural logarithm of the first uniform random number (generated early and stored in data register 08) multiplied by negative two. This product remains in the display register for manipulation. Calculation continues.

The squareroot of the previous operation end value is multiplied by the desired standard deviation. Finally, this product is added to the desired mean, resulting in the generated normal random number. Seed manipulation for the generation of successive normal random numbers is completed during the SBR D.MS portion of the normal generation program.

# 3. SBR 2nd D.MS

The TI 59 ML 15 program does compile statistical data to allow computation of the mean and standard deviation of the pseudo-random numbers generated when using the normal distribution routine and the

uniform distribution routine over ranges other than 0-1. However, these data are not compiled when SBR 2nd D.MS sequence is executed to produce uniformly distributed numbers over the 0-1 range. Data registers one through eleven are used by the ML-15 program to compile and compute these statistics. Hence, if this program is called to produce normal random numbers within a larger program, such as a simulation, the use of these eleven data registers must be forgone. Yet, if the ML-15 program is called only to produce uniform random numbers over the range 0-1, only data registers seven and nine are used by ML-15, freeing nine registers for other use. This aspect of the TI 59 ML-15 program must be carefully considered when utilizing it is as a subroutine within another program.

#### C. COMBAT MODELS

Today there are considered to be three types of combat models in use; war games, pure simulations and analytical models. War games are models and games Ref. 2 :

"... in which individuals simulating decision makers in real life use their judgement to perform the decision functions in the model."

A war game may include automation to assist in the processing of data and the generation of random numbers to determine the outcome of certain chance events. A war game may also be a player-assisted simulation where players provide input to a computer model based on output (readouts) during a simulated battle. In comparison with the other models, war games appear to be more realistic, involve greater player interaction, are less automated, require much more time to run, more resources and involve a smaller degree of abstraction.

Simulation combat models are models Ref. 2 :

"... which run completely without human intervention. In this type of model events in the different combat processes are based on predetermined rules which are programmed into the automated evaluation procedure."

Combat models of this type generally contain a significant number of the important stochastic elements of combat in an attempt to simulate real battle. These models use probability distributions for the many chance input variables and produce probability distributions as results.

They utilize the Monte Carlo technique, repeatedly sampling all input distributions in the programmed sequence to produce a distribution of probable battle results for each set of input data.

Analytical models are models Ref. 2 :

"... comprised of sets of mathematical equations as models of all the basic events and activities in the process being described and an overall assumed mathematical structure of the process into which the event or activity descriptions are integrated."

While analytical models are the most time efficient they are also the most abstract and difficult to understand. As with the pure simulation, there is no human intervention when an analytical model is used.

All three models represent abstractions of the real world. The models themselves can be observed more conveniently than the real world and theories about the real world can be developed by studying the results of these models. Subsequently, these theories can be used to make predictions about real world events.

Each model type has strengths and limitations, some noted above and others listed in table 2-4  $\begin{bmatrix} Ref. & 2 \end{bmatrix}$ .

## 1. Pure Combat Simulations

Pure combat simulations are normally viewed as production tools, using Monte Carlo techniques to obtain results enabling the prediction of future system performance. But because the real world is so complex and interactive, attempts to model every detail of a large system in a pure simulation and to include every element that may influence the system can result in simulations so large and so complex that they are understood only by their developers and not by other users or decision makers. To avoid this complex dilemma, analytical models can be used to represent elements of the system being modeled instead of simulating the element itself and its inherent stochastic processes with every trial. This technique has been followed to some degree in the pure simulation model presented in Chapter III where the calculation of detection probability is an analytical model with results based on target range.

It should be noted that few, if any, simulation models ever completely include all those elements and events that affect the system(s) under study. Reference 2 points out that:

". . . a model is always incomplete, with only those aspects represented that we believe we know well enough to model and that we consider important in the issues to be examined with the model. Obviously, models tend to be as simple and concise as our knowledge of the activity warrants."

This is reflected in the model presented in Chapter III. While all the factors affecting system performance have not been directly simulated they are included either as analytical models or as given in the scenario.

Finally, a point to be stressed is that simulations need not be large to be useful, nor require the use of a large electronic digital computer to be credible. Using large computers for large problems and small computers for small problems is a rule of thumb that may overstate the case but certainly does not exaggerate it. Use of the TI 59 as a computer to tackle the problem set forth in Chapter III is an example of matching the problem to the computing power required. It is also an excellent example of the computing power of the TI 59.

```
000
           76 LBL
          88 DMS
53 (
53 (
02 2
04 4
 001
002
003
                  <24300
 004
 005
 006
007
          02
09
08
65
43
 008
 009
                  X
 010
                ROL
          09
85
09
 011
                 09
012
013
                  +
                  9000
 014
          09
015
016
017
018
019
020
021
022
          09
          09
                                       TI 59 ML-15
          01
                  1
          54
                  )
+
1
                                       Program
          55
          01
                 9
          09
          09
          00
                 1
7
024
          01
025
026
027
          07
42
07
                STO
                 07
028
          54
029
          53
030
          53
031
032
033
          53
          22 INV
         59 INT
65 ×
43 RCL
07 07
034
035
036
037
         54
                 1
         42
09
55
038
               STO
039
                 09
040
                 ÷
```

TABLE 2-1.1

```
041
        43 ROL
042
        07
              07
043
        65
              \times
044
        05
              5
045
        22 INV
046
        28 LOG
047
        54
048
        59 INT
049
        55
             5
050
        05
051
        22 INV
        28 LOG
052
053
        54
       92 RTN
76 LBL
054
055
        13 C
71 SBR
056
057
        88 DMS
058
        53 (
24 CE
059
060
        65
061
             \times
062
063
        53
             (
        43 RCL
       11 11
75 -
43 RCL
064
065
066
067
068
        10
             10
       54 )
76 LBL
37 P/R
069
070
071
072
073
074
075
076
077
078
        85
        43 RCL
        10
             10
        54
        42 STO
       07
             -07
        78 I+
        43 RCL
07 07
080
        92 RTN
```

TABLE 2-1.2

```
081
  082
- X
- 2
+ X −
}
    119
120
TABLE 2-1.3
```

```
76 LBL
15 E
42 STO
09 09
92 RTH
76 LBL
121
122
123
124
125
126
127
128
139
130
131
132
133
134
135
136
137
                  11
                          Ĥ
                 42 STO
10 10
                92 RTN
76 LBL
12 B
42 STD
               11 11
92 RTN
00 0
                          Ū
               00
                           0
               00
                          Ō
               00
 140
               00
                          Ō
 TABLE 2-1.4
```

## TI 59 PROGRAM ML-15

# USER INSTRUCTIONS

# (MASTER LIBRARY MODULE)

| STEP | PROCEDURE                | ENTER | PRESS       | DISPLAY          |
|------|--------------------------|-------|-------------|------------------|
| 1    | SELECT PROGRAM           |       | 2d PGM 15   |                  |
| 2    | INITIALIZE               |       | 2d E'       | J                |
| 3    | ENTER RANDOM NUMBER SEED | SEED  | E           | SEED             |
|      | (0 ≤ SEED ≤ 199017)      |       |             |                  |
|      | FOR NORMAL DISTRIBUTION  |       |             |                  |
| 4    | ENTER DESIRED MEAN       | x     | A           |                  |
| 5    | ENTER DESIRED STANDARD   |       |             |                  |
| }    | DEVIATION                | -     | В           |                  |
| 6    | GENERATE RANDOM NUMBER   | }     |             |                  |
|      | (REPEAT AS NEEDED)       |       | 2d C'       | RANDOM<br>NUMBER |
|      | FOR UNIFORM DISTRIBUTION |       |             |                  |
|      | RANGE (0, 1)             |       |             |                  |
| 7    | GENERATE RANDOM NUMBER   |       |             |                  |
|      | (REPEAT AS NEEDED)       |       | SBR 2d D.MS | RANDOM<br>NUMBER |

## TI 59 PROGRAM ML-15

## DATA REGISTER CONTENTS

# REGISTERS:

$$R_{01}$$
  $\Sigma y$ 

$$R_{02}$$
  $\Sigma y^2$ 

$$R_{04}$$
  $\sum X^2$ 

TABLE 2-3

### War Games

Simulations

Intelligent play of decision maker.

Stylized decision routines, usually fixed throughout game.

Intelligent use of intelligence.

Very limited use of intelligence.

Can plan engagement and moves in advance.

Very limited planning horizon.

Adapts maneuver to situation.

Very limited adapted maneuver routines.

Can play many tactical situations (employment, penetration, etc.).

Usually stylized maneuver, limited change in formations.

Insight is gained by understanding the particular rationale used in the decision process in single situations analyzed.

Insight is gained by repeating the analysis in many situations using different values for key parameters.

Controller determines existence of engagement and pace of play.

Predetermined scenarios and engagement rules -- combat very intense.

Very slow and costly in resources.

Faster to run after completely developed.

Very few situations can be examined.

Many situations can be played and the sensitivity of key variables can be tested.

Greatest visibility for the user.

Can include direct involvement by user.

Reference 1, FM 44-90, Headquarters Department of the Army, 1977

TABLE 2-4

### III. COMBAT SIMULATION USING TI 59

This is a probabilistic duel simulation model, a pure simulation of a combat air battle, designed to reflect the characteristics of the Improved HAWK air defense artillery system (battery) in the manual mode under attack by a single cruise missile of sustained altitude, speed and direction.

The program scenario and engagement rules are predetermined with no user input once the simulation run has begun. Insight may be gained and the sensitivity of key variables tested dependent upon the use of different values entered by the user for these variables during program initialization. (Variables listed under E below.)

The model provides IHAWK system status, target engagement events and battle results as they are determined/occur. Only two battle results are possible: a "KILL" of the cruise missile or a unit "PENETRATION" by the cruise missile.

Given the operational ready rates of the major subsystems of the IHAWK system, the  $P_{\rm SSk}$  (probability of single shot kill) and the mean and standard deviation of lock-on-to-target times, the model samples from the uniform and normal distribution to determine system status, IHAWK missile kill or no kill and lock-on times. Target detection is modeled as a function of target range and is represented as a linear relationship in the simulation.

This simulation was developed to exhibit the computing power of the TI 59 and to determine if one parameter under the control of the IHAWK

battery commander could significantly affect air battle results. This parameter was the tracking radar "lock-on-to-target" time which is a function of operator training given (1) a manual mode operation, and (2) perfect equipment. The sensitivity of battle results to varying lock-on times is listed under F below.

### A. IHAWK SYSTEM

To be effective, an air defense system must be able to detect, identify, engage and destroy an airborne target. The IHAWK system can engage and destroy a full spectrum of threat aircraft and missiles operating throughout a wide range of tactical speeds and altitudes. It can engage a multiple target threat as well as single targets. The system is effective from ground level up to altitudes of about 48000 feet and out to ranges of about 40 kilometers. The system can operate at night, under all conditions of weather and reduced visibility. It can function effectively in an ECM (electronic countermeasures) environment and is Ref. 1 . mobile using organic unit vehicles or helicopters some adverse weather and heavy ECM may diminish some system capabilities.

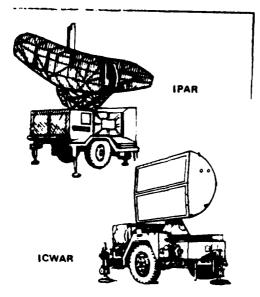
This simulation does not model: (1) weather

- (2) detection ECM
- (3) visibility
- (4) system mobility

## 1. Detection

Target detection is accomplished by either the improved pulse acquisition radar (IPAR) or the improved continuous wave acquisition radar (ICWAR), or both. The IPAR can detect low to medium altitude targets out to ranges in excess of 100 kilometers while the ICWAR can detect targets at very low altitudes with ranges in excess of 60





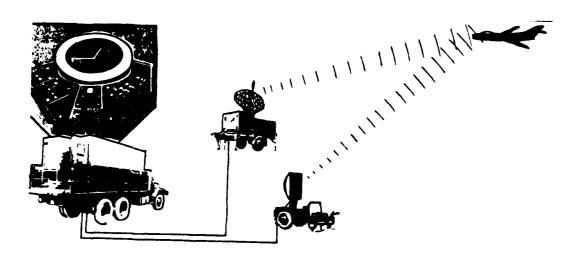


Figure 5-1

kilometers. Operating on the doppler principle, the ICWAR sees only very low moving objects and not stationary objects on the ground.

Detection may be reduced if terrain features such as hills, trees and buildings mask the radar's view of the approaching target. Even with completely level terrain, the earth's curvature causes a reduction in the detection and tracking ranges of the system against very low-altitude targets. Also, evasive maneuvers by threat targets may reduce the detection and tracking ranges and increase system response time, thereby reducing the effective or intercept range. This simulation does not

model:

- (1) terrain features
- (2) curvature of the earth
- (3) evasive action by targets
- (4) pulse detection or continuous wave detection per se

### This model assumes:

- (1) clear weather
- (2) no detection electronic countermeasures
- (3) line of sight (LOS) exists between radar and target
- (4) flat desert terrain
- (5) nonmaneuvering target
- (6) only one attacking target exists
- (7) target is a cruise missile of constant speed and constant altitude
- (8) detection is a function of target range

The probability of detection is modeled during each sweep of the radar as a linear function of target range from the battery as follows: For the IPAR the  $P_{DET} = (-.25 \div 65)$  \* Target Range + 1.0 For the ICWAR the  $P_{DET} = (-.5 \div 65)$  \* Target Range + 1.0 The probability of detection is calculated every three seconds of simulated time. This is based on the radar rotation rate of 20 revolutions per minute. That is, every three seconds each radar takes a 360 degree glimpse of the horizon. The radars are slaved to

each other and rotate in synchronization. Additionally, the IPAR is modeled to detect only targets from 5000 to 40000 feet in altitude while the ICWAR detects targets from 1 to 8000 feet in altitude. Thus the battery's very low and low to medium detection capability is dependent upon the operational status of these radars as noted. Targets above 40,000 feet cannot be detected in this simulation. The operational ready rates of these two radars has been arbitrarily set at .65 (ICWAR) and .95 (IPAR).

## 2. Identification

Identification of any potential target is accomplished by means of the identification, friend or foe (IFF), equipment of the IHAWK system and/or other established hostile criteria. If the target cannot be positively identified in this simulation because of a non-operational IFF, the target speed and altitude is checked to determine target status (foe or not foe). That is, if the IFF is nonoperational and if the target is below 5000 feet altitude and greater than 550 KMPH in speed, it is identified as a foe; otherwise, it is not a foe.

This model assumes: (1) once identified as a friend, always a friend, (2) once identified as a foe, always a foe.

The operational ready rate of the IFF has been arbitrarily set at 95 percent. This model does play IFF accuracy to the degree that an operational IFF will be in error two percent of the time. That is, a foe will be shown to be a friend two percent of the time. This model assumes operational IFF accuracy to be 98 percent.

**1** Identify

Figure 3-2

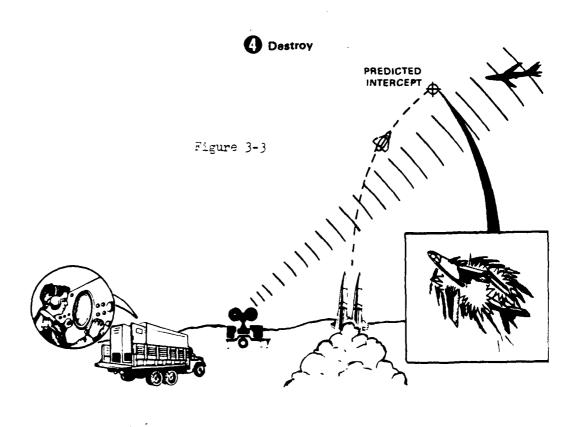
— CORRECT RESPONSE (FRIEND) —

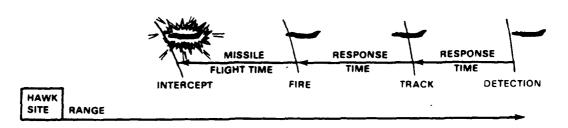
NO RESPONSE OR INCORRECT RESPONSE (FOE)

Engage

## Engagement/Destruction

The IHAWK battery has two firing sections, each of which contains a target tracking radar which is called an improved high powered illuminating radar (IHIPIR), and three launchers with three missiles each. If a potential target is determined to be a foe, it is assigned to one or both of these firing sections. The tracking radar of these sections, under the control of a fire control operator (enlisted personnel), attempts to lock-on to the approaching hostile target. The operator directs the automatic box search of the radar in the azimuth and expected elevation of the target in attempting this target lock. The operator's ability to achieve a target lock is a function of his training given the condition mentioned above. The time that elapses in attempting this target lock is extremely important. Target engagement cannot continue without target lock and the longer it takes to achieve target lock the closer the target moves toward the battery, reducing the intercept range. Tracking radar lock-on times are assumed to be normally distributed. After target lock has been achieved and the target is in range, one or two missiles are fired on order from the unit tactical control officer in a battery control van. Engagement is continued until the target is destroyed or until engagement is no longer possible. This simulation models each firing section as an entity. After a target has been declared a foe and assigned to one or both firing sections, this model simulates the target lock-on time by utilizing the TI 59 normal random number generator based on a normal mu and sigma input by the user during initialization.





The range at intercept is determined by the range at which detection and tracking (lock-on by the HIPIR) occur and on system response time.

In this model, targets are engaged that are:

- (1) declared to be foe
- (2) less than 40 KM from the battery
- (3) greater than 8 KM from the battery

## This model assumes:

- (1) two independent firing sections
- (2) salvo fire occurs if both sections are operational and shoot-look-shoot if only one section is operational
- (3) firing continues until kill or penetration
- (4) penetration means that the target is 8 KM or less from the battery
- (5) lock-on-to-target time is a function of operator training and is normally distributed
- (6)  $P_{ssk} = .75$  (arbitrarily set)

The operational ready rate of each firing section has been arbitrarily set at 75 percent.

## 4. Target

The target for this model is assumed to be a hostile cruise missile that flies straight in toward the battery at a constant speed and altitude as established by the user during initialization. The initial range of the target is also a user input. The lethality of the missile warhead is assumed to be such that any successful penetration by the missile to within 8 KM or less of the battery before destruction is considered a total penetration of the battery defended area. Therefore, the target must be destroyed before 8 KM to score a kill. Additionally, a target will not be engaged after detection until it is less than 40 KM from the battery and no further missiles will be fired at the target once it is within 8 KM of the battery. The target speed has a lower bound of 100 KMPH but no upper bound. Only targets between 1 and 40000 feet in altitude can be detected and are thus the altitude bounds. Finally, all targets are hostile and will be engaged

unless erroneously identified as friendly or not foe, resulting in a free penetration.

## 5. Time

This simulation is a time step model, updating all battery events and functions every three seconds of simulated time. This three-second interval stems from the rotation rate of the detection radars, 20 revolutions per minute or one complete rotation (scan of the horizon) every three seconds.

### B. MACRO FLOW CHART

The enclosed macro flow chart, figure 3-4, depicts the general flow of the simulation logic from start to either penetration or kill.

First the model determines if a detection capability exists. This could be one or both of the detection radars. Using the internal random number generator of the TI 59 for a 0-1 uniform distribution, two random numbers are drawn and compared with the detection radar operational ready rates. If the random number is less than the rate, the radar is operational; otherwise, it is nonoperational. If no detection capability exists the simulation is terminated by a penetration of the defended area by the target.

Detection of the target is based partly on the formulas set forth above and results of the 0-1 range uniform random number generator. The probability of detection is based on the range of the approaching target and is recalculated every three seconds. The probability of detection for each radar is compared with a generated random number between 0 and 1. If the random number is less than the probability

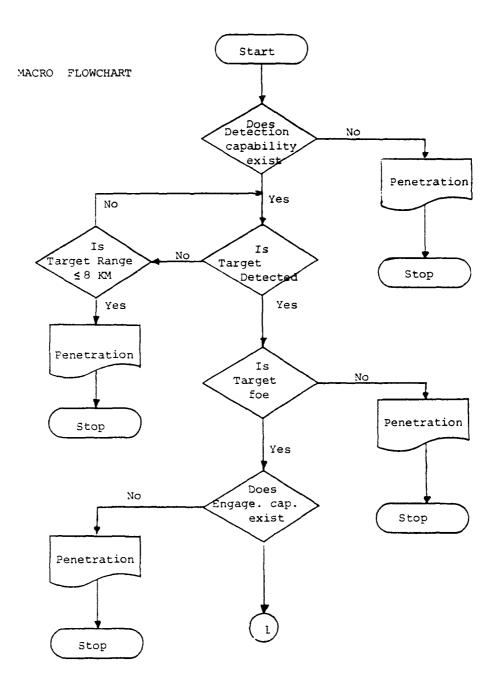


Figure 3-4.1

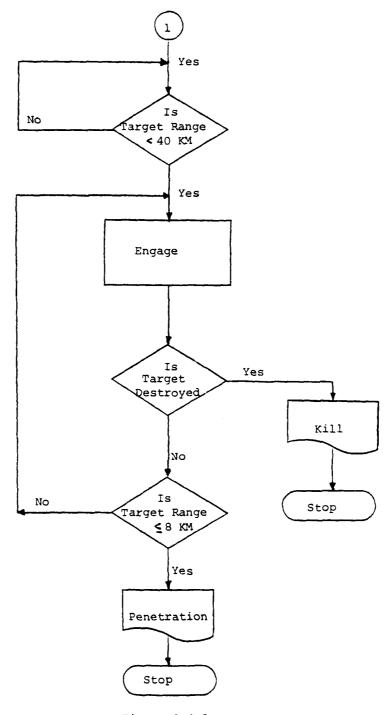


Figure 3-4.2

the target is detected; otherwise, it is not. As the target moves closer to the unit, the probability of detection increases linearly. However, detection is not based on range alone. The target must be within the detection altitude carability of the operational system. For instance, if the battery's detection capability rests solely on the IPAR because of a nonoperational ICWAR and if the approaching target is at an altitude of less than 5000 feet, detection will never occur and a penetration will result.

Identification of the target is determined by either the IFF or a combination speed and altitude envelope if the IFF is nonoperational. Operational status of the IFF is determined by comparing, again, a generated random number from a 0-1 range uniform distribution against the operational ready rate of the IFF. If the random number is less than the ready rate, the IFF is operational; otherwise, it is nonoperational. If the IFF is nonoperational and if the unit has a tracking capability, the target speed and altitude can be checked against an established hostile criteria. If the target is found to be below 5000 feet in elevation and above 550 KMPH in speed, it is designated a foe; otherwise, it is considered to not be a foe. Only targets positively identified as foes are engaged.

IFF positive identification of the hostile cruise missile as a foe is determined by comparing a random number generated from a 0-1 range uniform distribution against the IFF accuracy rate of 98 percent. If the random number is less than the accuracy rate, the cruise missile is correctly identified as a foe; otherwise, it is erroneously classified as a friend resulting in a penetration of the defended area.

The battery's engagement capability lies with its two firing sections, each tracking and firing on approaching hostile targets. Again, two random numbers drawn from the 0-1 uniform distribution are compared to the operational ready rates of the firing sections to determine the status as in the previous subsystems examples. If an engagement capability is determined to exist, the process continues on to direct missile firings at the target following target lock by the tracking radar(s). As mentioned earlier, this lock-on time is a function of operator training in the manual mode and is normally distributed. For highly trained operators the mean is assumed to be ten seconds with a standard deviation of five seconds. The lock-on time for each section is determined by two random numbers generated by the TI 59 random number generator from a normal distribution with mean and standard deviation determined by the user during program initialization. (Any random number less than zero is discarded and another generated to avoid negative times.) The length of the lock-on period directly affects the resultant target intercept range. If the lock-on time is sufficiently long the missile firing is delayed and the probability of a penetration is likely. (The determination of air battle results to varying lock-on times provided the basis for the development of this simulation, though other variables of the model can easily be tested for outcome sensitivity.) Again, targets are not engaged until less than 40 KM from the battery and no missiles are fired after the target is 8 KM or less from the battery.

Missile effectiveness after firing is determined when the IHAWK missile range equals or exceeds the cruise missile range from the

battery. A random number from a 0-1 range uniform distribution is generated for each missile fired and checked against the  $P_{\rm SSK}$ . Random numbers less than the  $P_{\rm SSK}$  result in kills while all others result in no kills. Engagement of the target continues until a kill or penetration is registered.

## C. MICRO FLOWCHART

The micro flowchart in appendix A depicts the detailed flow of processing throughout the simulation from start to kill or penetration.

D. SUBROUTINES, LABELS, FLAGS, DATA REGISTERS AND PROGRAM MEMORY STEPS

# 1. Subroutines and Labels

This simulation uses 49 of the 72 labels available for programming on the TI 59. Of these 49, 14 are subroutines. The remaining labels are used to identify sections of the program and to direct action to these sections during simulation runs. A complete listing of all labels is displayed in table 3-1 with the subroutines marked by an asterisk. Comments on selected labels and a printout of the entire program is enclosed in appendix A.

# 2. Flags

Nine of ten available flags are used. As the IHAWK equipment and target friend/foe status is determined, this model uses TI 59 flags to maintain a record of the system and target status. These flags subsequently direct the flow of processing and determine actions to be taken within the simulation engagement.

Flag 1 set means the target has been detected. Flag 2 set means the target is a friend. Flag 3 set means the ICWAR and the IPAR

are operational. Flag 4 set means only the ICWAR is operational. Flag 5 set means only the IPAR is operational. Flag 6 set means the IFF is operational. Flag 7 set means that alfa firing section is operational and bravo firing section is nonoperational. Flag 8 set means that bravo firing section is operational and alfa firing section is nonoperational. Flag 0 set means that both firing sections are operational.

# 3. Data Registers

The TI 59 memory storage area is initially partitioned to provide 60 data storage registers and 480 program storage locations. However, the user can repartition the memory storage area to suit his particular programming needs. The IHAWK simulation requires exactly 800 program memory locations and 20 data storage registers. Within the TI 59 there are a total of 120 registers to be used for data storage and program locations. While each register can store only one datum point, each can store eight program instructions or steps. Thus 3 \* 60 = 480 program locations which are initially available as mentioned above. Repartitioning the core 120 registers is done in increments of ten. Hence, to get the 800 program steps for the IHAWK simulation 100 core registers are needed. This leaves exactly the 20 needed for data storage.

To partition the storage area, the number of sets of 10 data registers needed is entered and 2nd OP 17 pressed. Thus for the IHAWK simulation, twenty data registers are available after the initial repartitioning by pressing 2 2nd OP 17. The registers and their contents are listed on the following page.

- $R_{\text{OO}}$  Target range. Entered by user.
- $\rm R_{O1} = R_{O1}$  through  $\rm R_{O8}$  are used by the TI 59 random number generator program.
- R<sub>02</sub>
- R<sub>03</sub>
- R<sub>04</sub>
- R<sub>05</sub>
- R<sub>06</sub>
- R<sub>07</sub>
- R<sub>08</sub>
- $R_{09}$  SEED for random number generator. Entered by user.
- R<sub>10</sub> Mean lock-on-to-target time. Entered by user.
- $R_{11}$  Standard deviation of lock-on-to-target time. Entered by user.
- $R_{12}$  IHAWK missile range from battery. Initially zero.
- R<sub>13</sub> IHAWK missile range from battery. Initially zero.
- $R_{14}$  Probability of detection work register.
- R<sub>15</sub> Target speed. Entered by User.
- R<sub>16</sub> Target altitude. Entered by User.
- $R_{17}$  Target range work register. Not entered by user.
- $R_{18}$  Simulation trials or runs to be completed. Entered by user.
- ${\bf R_{19}}$  Simulated time in seconds for each trial. Initially zero for each trial.

## 4. Program Memory Steps

There are 800 program steps available. All 800 program memory steps are used in this program.

### E. USER INSTRUCTIONS

The enclosed user instructions, table 3-2, provide the necessary steps to initiate a sequence of simulation runs. The enclosed printout results, table 3-3, indicate the 22 possible print statements that may occur during the simulation. A sample of data input and simulation run results are displayed in tables 3-4 and 3-5.

Two steps of the user instructions warrant further comment.

## 1. Step 2 Clear Data Registers.

Instead of clearing all data registers the user may wish to clear selected registers when repeating simulation runs as in the case of sensitivity analysis work. In this instance the user may just clear registers  $R_{01}$ ,  $R_{12}$ ,  $R_{13}$ ,  $R_{17}$ ,  $R_{18}$ ,  $R_{19}$  and enter the desired values.  $R_{09}$  need not be reentered as the program automatically changes the seed after each random number is generated. If the user does clear all data registers with 2d CMs the user must then enter an entirely different seed in  $R_{09}$  within the bounds noted.

# 2. Step 9 Check Data Register Content

This step is a quick safeguard for the user to ensure that the simulation run is based on the correct parameter values. This step provides a complete listing of the 20 data registers with contents for review prior to the final user step.

## F. SENSITIVITY ANALYSIS RESULTS FOR LOCK-ON TIMES

Four hundred simulation runs were made with four lock-on mean values: 10, 20, 30 and 40 seconds. In each case the lock-on time standard deviation was five seconds. For each simulation run the

target was initially set at a range of 50 KM in  $R_{00}$ , target speed was 1500 KMPH and target altitude was 7000 feet. An initial random number seed was entered for run number one but no further user seeds were provided, thus leaving seed manipulation to the program.

The results listed below indicate that air battle results are indeed sensitive to target lock-on times.

| LOCK-ON TIME |       | PENETRATION | KILL |
|--------------|-------|-------------|------|
| mu           | sigma |             |      |
| 10           | 5     | 11%         | 89%  |
| 20           | 5     | 14%         | 36 ⅓ |
| 30           | 5     | 26%         | 74%  |
| 40           | 5     | 44%         | 56≹  |

The results indicate a significant increase (12 percent) in defended area penetrations for a mu of 30 under the present scenario. This trend continues at an apparent exponential rate. With a mu of 40 seconds, defended area penetrations increase another 18 percent. Based on these results it appears advisable to maintain such a state of operator training that the mean target lock-on times be twenty seconds or less with as little deviation among the operators as possible. Furthermore, it seems that for the extra training assumed to be required to reduce mean lock-on times from 20 to 10 seconds there appears to be only a small marginal reward in the reduction of defended area penetrations (3 percent).

## G. RECOMMENDATIONS

While the intent throughout the thesis is to exemplify the capabilities of the TI 59 as a viable, real world analytical tool, the results of the TI 59 simulation lend insight into an area that requires

further investigation, that being IHAWK target lock-on times. While only the lock-on times themselves were varied for this simulation, other important scenario parameters should be varied to acquire an improved understanding of how air battle results can be affected by lock-on times.

Future enhancements of these results would include a significant increase in simulation runs for a wide variety of scenario parameter settings. While this TI 59 model allows certain parameter variations during program initialization, other parameters such as acquisition radar altitude detection capabilities can be varied with only minor adjustments to the program.

Regardless of whether future simulation studies are conducted using this TI 59 model or a facsimile on another computer, the results above warrant further research in this area.

```
COS
TAN
         39
 930
 045
         30
              DEG
 060
         БÜ
         69
17
 067
              ٦٢
 099
135
158
170
              €: •
         98 AD:
         90 LST
         42 STD
         18 0
 180
 203
208
222
231
235
              D
         14
         16 A*
         43 RCL
33 X2
         15 E
52 EE
 251
259
278
         10 E'
         19 D'
67 E
              Εū
 297
         88 DMS
 318
 334
338
         34 ∫%
         23 LNX
 354
         24 CE
         22 INV
32 X:T
25 CLR
28 LDG
38 SIN
37 P/R
 359
378
 393
 411
 455
*491
 502
          49 PRD
 510
          11
                A
               535
560
          12
13
         50 I I
*585
          89
79
*601
*639
*654
*656
*656
          59 INT
          48 E.KC
          80 GRD
70 RAD
                                 Table 3-1
          68 NOP
 667
677
          97 DSC
58 FIX
*685
          57 ENG
*708
          29 CF
*722
*731
*745
          96 WRT
          78 1+
          35 1/3
              Y H
*760
          45
  766
          44 SUM
```

| USER INSTRUCTIONS |   |  |                    |                   |
|-------------------|---|--|--------------------|-------------------|
| STEP              | PROCEDURE   | ENTER                                      | PRESS              | DISPLAY           |
| 1                 | REPARTITION   | 2  | 2d OP 17           | 799.19            |
|                   | 800 PROGRAM MEMORY<br>LOCATIONS<br>20 DATA MEMORY<br>REGISTERS  | :  |                    |                   |
| 2                 | Enter magnetic program cards, sides 1 through                   |  |                    |                   |
| 3                 | CLEAR DATA REGISTERS  |  | 2nd CMs            | (NO CHANGE)       |
| 4                 | RESET ALL FLAGS AND<br>CLEAR ALL SUBROUTINE<br>RETURN REGISTERS |  | RST                | (NO CHANGE)       |
| 5                 | ENTER IHAWK SYSTEM DATA   |  |                    |                   |
| ,                 | TRACKING RADAR "LOCK-ON" TIME                                   | n.   | STO 10<br>STO 11   | n<br>T            |
| 6                 | ENTER CRUISE MISSILE<br>DATA                                    | RANGE (KM)<br>10 < KM < 100                | GTO 777 LRN<br>LRN |                   |
|                   |   | RANGE (KM)                                 | <b>STO</b> 00      | RANGE             |
|                   |   | 10 < KM < 100<br>SPEED<br>ALTITUDE<br>(FT) | STO 15<br>STO 16   | SPEED<br>ALTITUDE |
| 7                 | ENTER SEED FOR RANDOM NUMBER GENERATOR (0 ≤ S ≤ 199017)         | SEED                                       | STO 09             | SEED              |
| 8                 | ENTER DESIRED NUMBER OF SIMULATION RUNS                         | #  | STO 18             | #                 |

Table 3-2.1

| USER INSTRUCTIONS |                                |       |                       |                               |
|-------------------|--------------------------------|-------|-----------------------|-------------------------------|
| STEP              | PROCEDURE                      | ENTER | PRESS                 | DISPLAY                       |
| 9                 | CHECK DATA REGISTER<br>CONTENT | 0     | RST<br>INV 2d<br>LIST | 0                             |
| 10                | START SIMULATION RUN           |       | LIST<br>R/S           | (SEE<br>RESULTS<br>POSSIBLE)* |
|                   | * PC-100 C PRINTER REQUI       | RED   |                       |                               |

Table 3-2.2

# RESULT PRINTOUTS

| NUMBER PRINTED | MEANING  |
|----------------|--|
| 1              | CRUISE MISSILE HAS BEEN DETECTED AT (RANGE GIVEN IN KMS FROM UNIT)                                     |
| 3              | LOW ALTITUDE DETECTION RADAR (ICWAR) AND MEDIUM ALTITUDE DETECTION RADAR (IPAR) ARE BOTH OPERATIONAL   |
| 4              | ONLY ICWAR IS OPERATIONAL  |
| 5              | ONLY IPAR IS OPERATIONAL   |
| 6              | IDENTIFICATION FRIEND-OR-FOE (IFF) IS OPERATIONAL  |
| 7              | ALFA FIRING SECTION IS OPERATIONAL, BRAVO FIRING SECTION IS NONOPERATIONAL                             |
| 8              | BRAVO FIRING SECTION IS OPERATIONAL, ALFA FIRING SECTION IS NONOPERATIONAL                             |
| 9              | BOTH FIRING SECTIONS ARE OPERATIONAL   |
| 10             | CRUISE MISSILE IS IDENTIFIED AS A FOE  |
| 11             | BRAVO FIRING SECTION IS FIRING ONE MISSILE AT A TARGET < 40 KM FROM THE BATTERY, BUT GREATER THAN 8 KM |
| 12             | ALFA FIRING SECTION IS FIRING ONE MISSILE AT A TARGET <40 KM FROM THE BATTERY, BUT GREATER THAN 8 KM   |
| 14             | CRUISE MISSILE IS ERRONEOUSLY IDENTIFIED AS A FRIEND BY IFF  |
| 15             | CRUISE MISSILE IDENTIFIED AS NOT FOE BY SPEED AND ALTITUDE CRITERIA, IFF IS NONOPERATION               |
| 17             | ALFA FIRING SECTION IS OPERATIONAL   |
| 18             | ALFA FIRING SECTION IS NONOPERATIONAL  |
| 23             | BATTERY IS NONOPERATIONAL, NO DETECTION CAPABILITY   |
| 24             | BATTERY IS NONOPERATIONAL, NO FIRING CAPABILITY  |
| 25             | ALFA SECTION MISSILE "NO KILL" FOLLOWED BY RANGE (KM) OF APPROACHING TARGET                            |

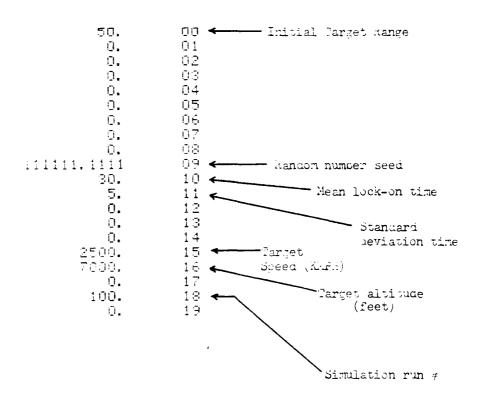
Table 3-3.1

# RESULT PRINTOUTS

| NUMBER PRINTED | MEANING  |
|----------------|--|
| 26             | BRAVO SECTION MISSILE "NO KILL" FOLLOWED BY RANGE (KM) OF APPROACHING TARGET |
| 66             | IFF IS NONOPERATIONAL  |
|                | •  |

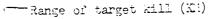
TARGET "KILLS" ARE SPELLED OUT, I.E. "KILL", FOLLOWED BY THE RANGE FROM THE UNIT AT WHICH THE TARGET WAS DESTROYED

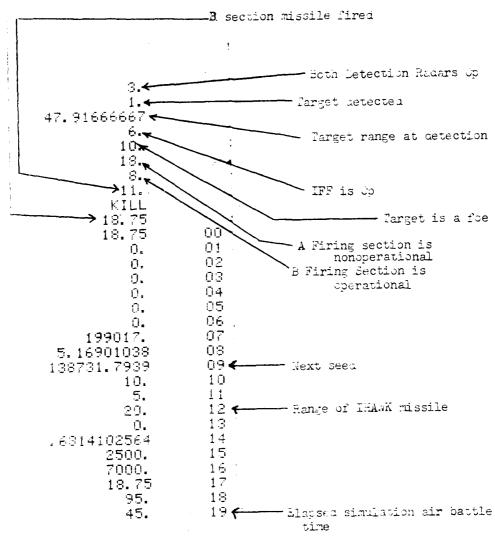
"PENETRATION" IS PRINTED WHEN A CRUISE MISSILE APPROACHED WITHIN 8 KMs OF THE BATTERY. IN THIS INSTANCE THE UNIT IS CONSIDERED PENETRATED AND DESTROYED



Farameter Value Inputs To Selected Data Registers

Pable 3-4





Printout During Simulation an: Data Register Contents Pable 3-5

# IV. DATA ANALYSIS

#### A. PURPOSE

The purpose of this chapter is to demonstrate how the TI 59 may be used to analyze data. Rather than use assumed or contrived data, an actual experiment was conducted by the authors for illustrative purposes. Strict requirements for random sampling were not met in conducting the experiment but, again, the purpose of this thesis is to demonstrate the capabilities of the TI 59 rather than to make inferences or draw broad conclusions from the experimental data.

Before discussing methods for data analysis, the scope, design, and methodology of the experiment will be presented in sufficient detail to make the data analysis meaningful. Presentation of the experiment will be followed by a detailed discussion of a TI 59 program designed to compute measures of central tendency and spread for sample data. Chapter V discusses a TI 59 program which may be used to make statistical inferences using the same experimental data.

# B. FITNESS EXPERIMENT

# 1. Scope of the Experiment

The experiment was conducted to test the hypothesis that different physical conditioning programs result in different levels of physical fitness. Six different conditioning programs were evaluated using five tests. The scope of the experiment was limited to testing the strength and endurance of selected upper body muscles, together with overall cardiovascular fitness. A completely comprehensive fitness

evaluation would also include lower body strength and endurance as well as muscular flexibility and agility. Other factors such as diet, use of alcohol, tobacco and other drugs would also be requisite. This experiment was limited to the examination of thirty-six male subjects by the two authors to determine cardiovascular efficiency, bicep strength, bicep endurance, pectoral strength and pectoral endurance. Thirty of the subjects were military officers attending the Naval Postgraduate School. The other six subjects were weightlifters who trained at Bailey's Gym in Seaside, California. The subjects varied in age from nineteen to thirty-seven but were predominantly in their early thirties. While it is recognized that strict requirements for random sampling requisite for statistical analysis were not met in conducting the experiment, it should be pointed out that there is every reason to believe that the subjects examined were representative of the population from which students are continually drawn for the institution. Strict inference to any specified population will not be made, but as mentioned earlier the purpose of this discussion is to illustrate the use of programs developed for the TI 59, not to make inferences from the data gathered in this particular experiment.

Since the terms, strength, endurance, and cardiovascular efficiency are subject to a myriad of interpretations, the definitions used for this analysis are presented before proceeding to discuss the test methodology. Muscular strength is defined as the ability to exert maximum force against an object, while muscular endurance relates to the ability to exert force which is not necessarily maximal over an extended period of time. Cardiovascular efficiency relates to how

well the heart, lungs and blood vessels work together without strain  $\begin{bmatrix} Ref. 9 \end{bmatrix}$ .

Before analyzing the results a thorough explanation of the experimental design and methodology is provided.

# 2. Experimental Design

The subjects were divided into six categories (each consisting of six individuals) based on their exercise programs. The following six categories were used: Category I - Individuals who had participated in no exercise over the last six months; Category II - Individuals who ran more than thirty miles per week and who did so for at least the last six months; Category III - Individuals whose exercise consisted solely of lifting weights, whether for power or building physique, and who lifted at least twice a week; Category IV - Individuals who lifted weights at least twice a week, who ran twenty or more miles per week and who did both the lifting and running for at least the last six months; Category V - Individuals who lifted weights at least twice a week, who ran between ten and nineteen miles per week, and who did the lifting and the running for at least the last six months; and Category VI - Individuals who did not run or lift weights but who participated in basketball, racquetball, bicycling, or judo on a regular basis.

Five tests were administered to each subject in each category.

Cardiovascular efficiency was measured using the Pipes Test for Cardiovascular Health, which consists of the following seven steps:

- 1. Have the subject lie quietly on a pad for ten minutes.
- 2. Take a pulse reading for the resting heart rate.

- Have the subject sit on a chair with his arms folded across his chest.
- With his arms folded, have the subject stand up and sit down twice every five seconds for three minutes.
- Take a reading for the heart rate immediately after sitting down at the conclusion of the three minute exercise.
- Take readings at 30-second, 60-second, and 120second intervals after the exercise to measure recovery heart rate.
- Using a table developed by Pipes and the five heart rate readings determine the cardiovascular health score.

This test, developed by an exercise physiologist, [Ref. 9] is based on the premise that the heart rate describes an individual's fitness in three areas: how much oxygen he needs, how much blood his heart has to pump to meet the oxygen need, and how hard the heart works. Individuals with a low level of fitness do not extract oxygen efficiently from the blood so must pump more blood, resulting in a higher heart rate. In conducting the test, the same examiner took the pulse readings at the different intervals using the radial artery in the subject's wrist. The heart rate was monitored for ten seconds then multiplied by six to obtain the number of heart beats per minute.

The muscular strength test used for biceps was the maximum standing curl the individual could accomplish using a barbell. The proper technique was demonstrated to each subject by the examiner and lifts where the individual "cheated" by swinging the weight or arching his back were not counted. Bicep endurance was measured by the number of curl repetitions the subject performed with a 55 pound weight. These two tests were predicated on the generally accepted basis that curling

is the primary bicep exercise and that low repetition, high resistance exercises are best for developing endurance [Ref. 3]. Fifty-five pounds of weight were selected prior to the experiment as a low resistance weight well below each subject's strength capability and therefore in compliance with expert opinion that the force used for endurance testing should be considerably below the individual's static force capability [Ref. 7].

In a similar fashion, the bench press was used to test pectoral strength and endurance. Pectoral strength was measured by the maximum weight that the individual could bench press, while pectoral endurance was measured by the number of bench press repetitions he could perform.

Each subject was tested using an identical sequence of events. Initially each person was given an instruction sheet (table B-1 in Appendix B) which explained the purpose of the experiment and defined those attributes to be measured, i.e. muscular endurance, muscular strength, and cardiovascular health. The subject was then asked to complete a questionnaire (table B-2, Appendix B) concerning certain aspects of his medical history. Each man was instructed to stop the testing if he felt any significant level of pain. He was then asked to complete a form disclosing his name, age, weight, and height (table B-3, Appendix B). Next, one of the examiners questioned the subject concerning his exercise program over the last six months and made a subjective judgement as to which of the six categories he belonged in.

After this administrative procedure was completed, the actual testing was begun with the bench press test described above. (The

same examiner tested each of the thirty-six subjects in both the strength and endurance exercises in order to minimize any variance due to test administration.) The subject was shown how to do the bench press, allowed to practice once if desired, and then tested for the maximum number of repetitions he could perform with 100 pounds. The number of repetitions was recorded and the subject was allowed a three minute rest before being tested for his maximum bench press. The examiner estimated the amount that each subject could bench press and set up the weights accordingly. All adjusting of weight was done by the examiner so that the subject's lift capability was not degraded. The man was then asked to bench press the weight set up for him. If he was able to make the lift ten pounds were added and he was asked to try again. If he failed the second attempt he was given credit for five pounds less than he attempted. For example, if an initial attempt of 165 pounds was successful and a subsequent attempt of 175 pounds was missed, then the score was recorded as 170 pounds.

After another three minute rest the subject was tested on the number of times he could curl 55 pounds. This was followed by another three minute rest before testing for his maximum curl capability. Once again, the man's maximum lift was estimated by the examiner and all adjusting of the weight was done by the examiner.

Following the four lift tests, the Pipes Cardiovascular Health

Test [Ref. 9] was administered by the second examiner and the subject's testing was completed. Before examining the test results, a procedure for scoring the tests was requisite. Accordingly, the scoring procedure explained in the following discussion was decided upon.

## 3. Scoring Methodology

The heart rates recorded during the Pipes Cardiovascular Test were scored using table B-4 in Appendix B. Each subject's score for resting heart rate, heart rate immediately after the exercise and heart rate at the 30-second, 60-second, and 120-second intervals was aggregated to a total score ranging from zero to one hundred. This score was then used as the measure of cardiovascular fitness for comparative analysis.

In order to compare muscle strength among the subjects and among the categories, it was necessary to adjust each subject's lift for varying sizes and body structures. Accordingly, each man's maximum curl and maximum bench press were divided by his body weight, resulting in an adjusted score for each lift. These two adjusted scores were then added together to yield an upper body strength measure. For example, let S<sub>13</sub> be the strength measure for the third subject in Category I (where the first subscript indicates the category and the second indicates the subject within the category). The following formula may then be used to obtain the strength score for the third subject tested in Category I:

# S<sub>13</sub> = maximum bench + maximum curl body weight

As discussed earlier, muscle endurance was measured for the same two areas tested for strength - the biceps and the pectorals. The bicep endurance was measured by the maximum number of curl repetitions performed with 55 pounds, while the pectoral endurance was measured by the maximum number of bench presses accomplished with 100 pounds. As

in the case of strength, an adjustment was made for the subject's body weight. In the case of endurance, however, the amount of weight lifted (which was 55 pounds for the curl and 100 pounds for the bench press) was divided by the subject's body weight and then multiplied by the corresponding number of repetitions lifted. These two scores were then summed as the endurance index. For example, let  $E_{13}$  be the endurance score for the third subject tested in Category I. The following formula then obtains:

## 4. Test Results

Tables B-5 through B-10 in Appendix B reflect the results of the experiment for each of the six categories tested. For example, table B-5 depicts the age, weight, cardiovascular score, adjusted strength score and adjusted endurance score for each of the six subjects tested in Category I. Appropriate references are made at table B-5 for the development of the final cardiovascular, strength and endurance scores. The scoring methodology section of the chapter provides a detailed explanation of the rationale and methodology for deriving these scores.

# C. TI 59 PROGRAM FOR DATA ANALYSIS

Having developed the experimental design, the scoring methodology, and the test results it is now possible to analyze the data. Measures of

central tendency and spread will be used to illustrate an application of the TI 59 in analyzing sample data. The measures of central tendency used for this illustration are the mean,  $\overline{x}$ , and the median. The measures of spread used are: the sample variance,  $s^2$ ; the standard deviation, s; the mean absolute deviation, MAD: the mean squared deviation, MSD; the root mean squared deviation, RMSD; and the range. A TI 59 program will now be described in detail which computes these measures followed by an example applying the program to the results of the fitness experiment.

# 1. TI 59 Capabilities

The TI 59 has been hard-wired to calculate the sample mean and variance as well as MSD. As described in the TI 59 Personal Programming Manual Ref. 12 if each datum is entered into the calculator followed by pressing the  $\Sigma$ + key, the calculator will sum each data entry,  $x_1$ , into register one, sum the squares of  $x_1$  into register two, store the number of data entries in register three, and calculate  $\overline{x}$ ,  $s^2$ , and MSD. (By definition,  $s^2 = 1/n-1$   $\sum (x_1 - x)^2$  is the unbiased estimator for  $\sigma^2$  while MSD =  $(n-1)s^2/n$  is the maximum likelihood estimator.) Pressing the  $\overline{x}$  key will yield the mean, INV  $\overline{x}$  will display  $s^2$  and 2nd Op 11 will display MSD. If these are the only measures desired then utilization of the  $\Sigma$ + key is the most expedient method of obtaining them. The TI 59 statistics module has a program (Program 03) which computes these same measures as well as the middle value (MIDVAL). Additionally, Program 03 stores each data entry beginning with register 31. Program 03 also computes a number of other quantities not germane

to an analysis of the data gathered in the experiment discussed previously in this chapter. Since this results in a slightly longer run time for each computation, a program has been written by the authors which exploits the hard-wire capabilities of the  $\Sigma$ + key, computes MAD and range in addition to the other measures discussed, and stores the data for recall or transformation if desired. In addition, this program may be used with the TI 59 Master Module if the Statistics Module is not available. The following section describes the program in detail.

# 2. Univariate Data Program

In order to facilitate the description of this program a flow-chart (figure 4-1), has been included at the end of the chapter.

Comments in the paper are keyed to figure 4-1 by numbered circles for easy reference.

The program is initialized by pressing E' (figure 4-1, (1)). Initialization entails clearing all of the data registers, lowering flag 0 the purpose of which will be addressed later, and storing 31 in register 30. Register 30 is used as a post office for indirect addressing. In this particular program this means that data are stored in the register indicated by register 30. For example, after initialization, register 30 contains 31. The sequence  $\mathbf{x}_1$ , STO 2nd IND 30 will result in  $\mathbf{x}_1$  being stored in register 31. When the initialization routine, 2nd E', is complete the display will contain the value 31. Each datum may now be entered successively followed by pressing A. The routine at Label A begins by storing  $\mathbf{x}_1$  in a working, register 13 (figure 4-1, (2)).  $\mathbf{x}_1$  is then stored permanently beginning in register 31.  $\mathbf{x}_1$  is stored

in register 31, then register 30 the indirect storage address is incremented by 1 so that  $x_2$  will be stored in register 32,  $x_3$  in register 33 and  $x_n$  in register 31 + n - 1. A total of sixty-nine entries may be made using registers 31 through 99 for data storage. Registers 0 through 29 are used to make the requisite computations of central tendency and spread. After each datum,  $\boldsymbol{x}_i$ , has been stored, the program checks to see if flag 0 is raised (figure 4-1,(3)). If flag 0 is raised this indicates that a data entry has been made previously, ie., the current  $x_i$  is not  $x_j$ . In this event the program skips to Label x. If flag 0 is not raised, ie., the current  $\mathbf{x_i}$  is  $\mathbf{x_i}$ , then  $\mathbf{x_i}$  is recalled from the working register, register 18, and stored in register 12 as the minimum  $\mathbf{x}_i$  and register 13 as the maximum  $\mathbf{x}_i$ . Future entries may then be checked against register 12 to determine which value is lower. If a current  $\mathbf{x}_{\hat{1}}$  is lower than the value in register 12 then it will replace it as  $\mathbf{x}_{\min}$ . Similarly, subsequent entries may be checked against register 13 in order to retain  $\mathbf{x}_{\text{max}}$ . After storing  $\mathbf{x}_1$  in register 12 and in register 13 the program internally calls the key which, as disscussed previously, will sum  $\boldsymbol{x}_{i}$  into register 01, sum  $\mathbf{x_i}^2$  into register 02, sum the number of entries into register 03 and compute  $\overline{\mathbf{x}}$ ,  $\mathbf{s}^2$ , and MSD. Flag 0 is then raised so that subsequent entries will skip to Label x and replace  $x_{min}$  or  $x_{max}$  as appropriate. The program then recalls the number of entries, n, into the display and stops awaiting the next entry (figure 4-1,(4)). The second entry  $x_2$  will now be stored temporarily in the working register, register 18, and permanently in register 32. The indirect addressing register, register 30, is incremented by 1 for the next entry and the program then checks

to see if flag 0 is raised. Since this is not the first entry, the flag will be raised causing the program to skip to Label x (figure 4-1, (5)). The first step under Label x is to recall  $x_{\min}$  from register 12 and store it in the test register  $R_{T}$ . For this particular iteration,  $x_{s}$ will be in register 12 since the first entry was both the maximum and the minimum value processed as described earlier. The program then recalls the current  $\mathbf{x}_i$  ( $\mathbf{x}_2$  in this instance) from the working register, register 18. The display value,  $x_2$ , is checked against the  $R_T$  value,  $\mathbf{x}_1$ , to see if the display value is less than the  $\mathbf{R}_{\overline{\mathbf{x}}}$  value. If so the program skips to step 57 where  $x_2$  is stored in register 12, replacing  $x_1$  as the lowest data entry (figure 4-1, (6)). If the display value is not less than the  $R_m$  value then the program recalls  $x_{max}$  from  $R_{1,3}$  and stores it in  $R_m$ .  $x_i$  is recalled from the working register, register 18, into the display. This time the program checks to see if the display value,  $x_i$  is greater than the  $R_T$  value,  $x_{max}$ . If so, the program skips to step 62 where  $x_i$  is stored in register 13 as the new  $x_{max}$  (fig. 4-1, (7)). The program then computes the MIDVAL by recalling  $x_{\min}$  from register 12 and  $x_{\text{max}}$  from register 13, summing them and dividing by 2, and storing in register 14. Next the range is computed by subtracting  $x_{min}$  from  $x_{max}$ . The range value is stored in register 15 (figure 4-1, (3)). The program then loops back to the + key to compute the mean, variance and MSD, (figure 4-1,(9)). The number of entries is recalled and displayed awaiting the next entry. This process is repeated until all of the data have been processed.

The outputs of the program may be recalled as shown in table 3-11

in Appendix B. The mean is displayed by pressing  $\overline{x}$ , the variance by pressing Inv  $\overline{\mathbf{x}}$ , and MSD by pressing 2nd op 11. The lowest data point,  $\mathbf{x}_{\text{min}}$ , may be discovered by recalling register 12 while the highest data entry,  $\mathbf{x}_{\text{max}}$ , may be recalled from register 13. Recalling register 14 will display the MIDVAL and the range may be found by recalling register 15. Each of the original data entries may be recalled if desired beginning with  $x_1$  in register 31. MAD is computed by pressing 2nd A' which calls a different subroutine. This subroutine recalls  $\overline{x}$ which was computed under Label A and stores it in Register 16. The number of entries, n, is recalled from register 3 and stored in register 7 to be used as a decrement register. Register 20 contains 31 which is used to indirectly address the datum which have been stored beginning with register 31. The program recalls each  $x_i$  using register 20 and subtracts  $\overline{x}$ . The absolute value of the difference is summed into register 19. The program does this successively for each x; until the decrement register, register 20, is equal to zero indicating that each x; has been processed. The sum of the absolute values of the deviations from the mean is recalled from register 19 and divided by n which is recalled from register 3. This value, the mean absolute deviation is displayed completing the subroutine A' processing. All the values discussed earlier are still intact and may be recalled if needed. Table B-12, Appendix B, is a program listing for the univariate program.

## D. APPLICATION OF THE TI 59 UNIVARIATE PROGRAM

The cardiovascular scores for Category I provide a ready example for the use of the univariate program to calculate measures of central

tendency and spread. After the program card has been read in, the program is initialized by pressing 2nd E'. The cardiovascular scores for Category I (table 3-5) are entered into the calculator as follows: 56.5, A; 58, A; 58, A; 44.5, A; 33.5, A; 40, A. The instructions contained in table B-11 may then be used to obtain the desired statistics. For this particular example: 2nd x yields the mean, 48.4; RCL 14 displays the MIDVAL, 45.75; RCL 15 displays the range, 24.5; 2nd A' yields the mean absolute deviation, 9; 2nd Op 11 displays the mean squared deviation, 92.9; 2nd Op 11, $\sqrt{x}$  , calculates the root mean squared deviation, 9.6; INV 2nd  $\overline{x}$  recalls the standard deviation, 10.56; INV 2nd  $\overline{\mathbf{x}}$ ,  $\mathbf{x}^2$  calculates the variance 111.5; RCL 12 displays the lowest data entry, 33.5 and RCL 13 displays the highest data entry, 58. To calculate the sample statistics for another category or for a different test the user need only push 2nd E' to re-initialize and then enter the relevant data. Statistics have been calculated for the age, weight, cardiovascular scores, endurance scores, and strength scores for each of the six categories. Tables 4-1 through 4-6 display these statistics. Rather than discuss each of these tables in depth, one example is provided relative to the interpretation of the sample statistics.

The cardiovascular mean for Category I, 48.4, indicates average cardiovascular fitness using the Pipe's test which is based on a scale from 0 to 100. Three measures of spread (standard deviation 10.56, root mean squared deviation, 9.6, and mean absolute deviation, 9) are approximately equal to ten, a rather high variability in this case. The range, 24.5, also indicates that the data are quite spread out.

 $x_{\min}$  of 33.5 and  $x_{\max}$  of 58, the bounds of the sample data indicate that the cardiovascular fitness of sedentary people varies from poor to average.

Inferences, subject to the sampling limitations already discussed, may also be made about the strength or endurance of sedentary people using the data from table B-5. Similarly, the statistics for the other categories may be used to make inferences about the strength, endurance, or cardiovascular fitness of those who run over thirty miles per week (Category II) or those who lift weights (Category III) or any of the other three categories. Programs have also been written for the TI 59 which allow a user to develop confidence intervals for these sample statistics Ref. 14 .

The next chapter will discuss a program for one factor analysis of variance and then apply the program to the fitness data to illustrate statistical inference with the TI 59.

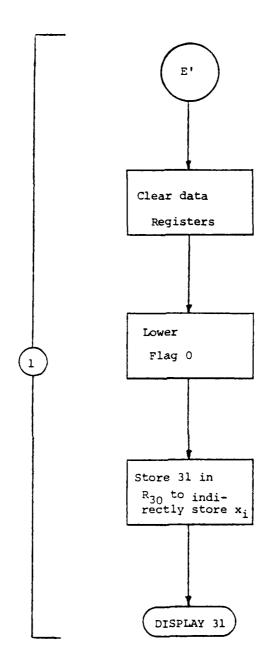


Figure 4-1.1

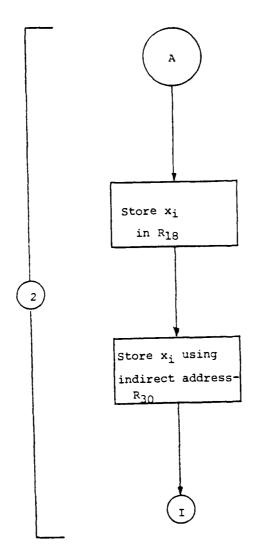
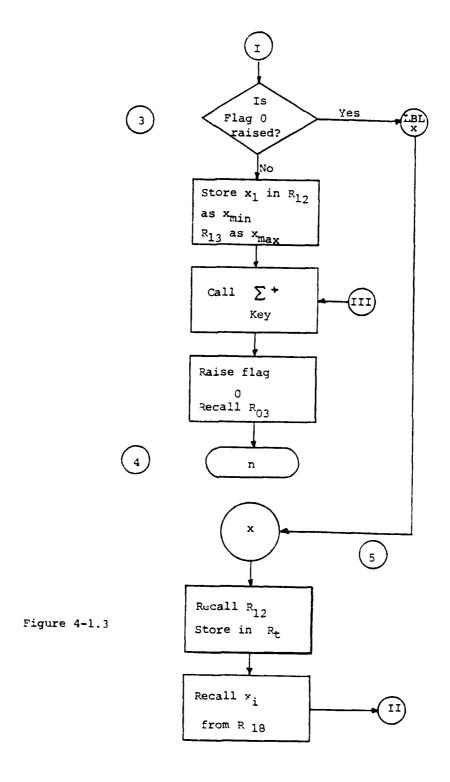
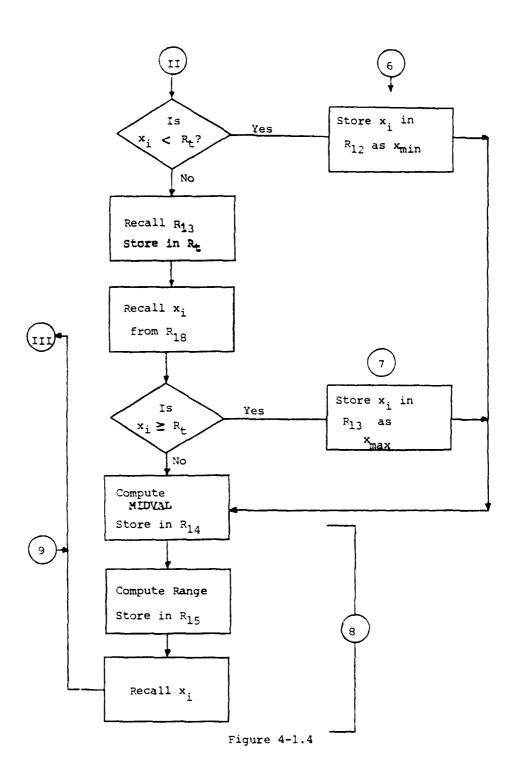


Figure 4-1.2





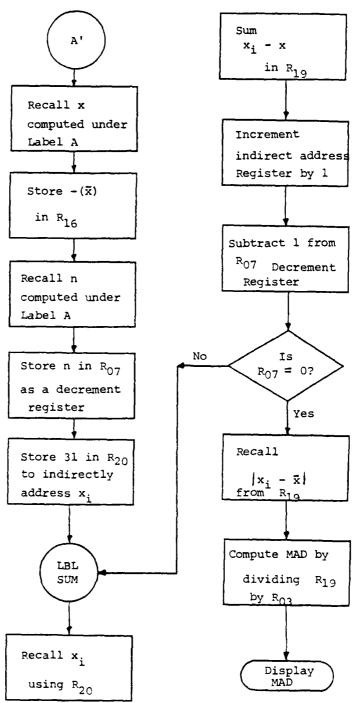


Figure 4-1.5

| X<br>max | 37.0  | 205.0  | 58.0            | 1.32              |
|----------|-------|--------|-----------------|-------------------|
| RMSD     | 2.74  | 18.58  | 09.6            | .11               |
| MSD      | 7.5   | 345.1  | 92.9            | .012              |
| ഗ        | 3.00  | 20.30  | 10.56           | .12               |
| 25       | 0.6   | 412.0  | 111.5           | .014              |
| MAD      | 2.30  | 16.40  | 00.6            | .085              |
| RANGE    | 8.00  | 50.00  | 24.50           | .35               |
| MIDVAL   | 33.00 | 180.00 | 45.75           | 1.15              |
| MEAN     | 33.3  | 172.8  | <b>11°8</b> 71  | 1.17              |
|          | A(E   | WEIGHT | CARDIO<br>SCORE | STRENCTH<br>SCORE |

155.0

33.5

Xmin

29.0

.97

5.5

27.9

8.00

63.9

8.70

76.7

7.17

22.40

16.70

15.25

ENDURANCE SCORE

TABI,E 4-1

TABLE 4-2

TABI,E 4-3

Xmin 180.0 22.0 24.5 2.0 31.6 Х 34.0 225.0 2,83 86.5 62.5 RMSD .255 4.06 14.6 110.0 10.49 20.5 .065 213.9 422.0 16.4 MSD 51: 17 .279 11.49 16.0 22.5 ß 19.76 .078 256.6 132.0 506.4 25 MAD .20 5.5 11.4 17.6 9.3 HANGE 12.0 .83 45.0 62.0 30.9 MIDVAL 47.05 28.0 202.5 2.42 55.5 52.25 MEAN 2.39 947.94 26.8 205.3 ENDURANCE SCORE STRENCTH SCOME WEIL;HT CARDIO SCORE AUE

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CATECOHY III STATISTICS

Xmin

X max

RMSD

19.0

32.0

4.58

25.5

28.0

A. A.

MEAN

160.0

240.0

26.7

200.0

187.5

WEIGHT

30

0.178

83.4

CARDIO SCORE

1.85

2.67

.27

34.3

0.64

6.4

144.38

ENDURANCE SCORE

2.23

STREWITH SCORE

71.5

96.5

8.1

TABLE 4-5

X 1.15 19.0 120.0 39.5 22.0 Х пах 205.0 2.43 35.0 77.5 54.1 RMSD 26.0 5.6 ¥. 11.8 12.2 .146 MSD 6.773 31.2 138.1 148.8 .419 13.4 28.5 6.1 12.9 S .176 37.5 813.0 165.7 178.6 22 MAD 4.7 19.3 .28 8.2 10.8 HA IV. E 16.0 1.2885.0 38.0 32.1 MIDVAL, 162.5 1.79 27.0 58.5 38.0 MEAN 171.5 1.83 7.82 92.8 34.4 ENDHRANCE SCORE STRENGTH SCORE CARD IO SCURE WELLIHT ACE.

CATECORY V STATISTICS

CATECORY VI STATISTICS

| X<br>i.m | 22.0      | 125.0  | 47.5             | 1.15              | 11.4               |
|----------|-----------|--------|------------------|-------------------|--------------------|
| X<br>nax |           | 205.0  | 86.5             | 1.56              | 23.1               |
| HMSD     | 3.56 1.89 | 23.7   | 14.1             | .016 .13          | 3.58               |
| MSD      |           | 561.8  | 199.9 14.1       | .016              | 12.8               |
| લ્ય      | 2.06      | 25.96  | 15.5             | .14               | 3.9                |
| న్న      | 4,26      | 674.2  | 239.9            | .020              | 15,38              |
| MAD      | 1.44      | 15.8   | 12.9             | .11               | 2.83               |
| HANGE    | 6.0       | 80.0   | 39.0             | .41               | 11.2               |
| MIDVAL,  | 30.0      | 165.0  | 0.59             | 1.36              | 17.25              |
| MEAN     | 30.7      | 170.8  | 50.9             | 1.36              | 16.6               |
|          | AGE       | WEFORE | CAHD 10<br>SCORE | STRENCTH<br>SCORE | ETUURANCE<br>SCORE |

∂2

## V. STATISTICAL INFERENCE

## A. PURPOSE

The purpose of this chapter is to illustrate a method of statistical inference using the TI 59. As in chapter IV the intent is to demonstrate the capabilities of the TI 59 rather than to emphasize statistical principles. One-way analysis of variance (ANOVA) will be used to demonstrate statistical inference using the fitness data discussed in the preceding chapter. The variations of the underlying populations represented by the six categories are assumed to be unknown but equal for this illustration.

### B. TI 59 PROGRAM FOR ANALYSIS OF VARIANCE

In testing the hypothesis that the population means for each of the six test categories are equal,  $H_0$  is typically rejected if the F ratio exceeds the critical F value in a standard table for the desired test level (typically 5%). Alternatively, using the TI 59 to its full advantage, prob-value may be used to test  $H_0$ . Prob-value is a method of testing whether or not the null hypothesis is supported by the data. In the case of the F ratio, prob-value is the probability that the F ratio would be as large or larger than the value actually observed if  $H_0$  were true. This is the right hand tail area, Q (f), where

$$Q(f) = Pr (F > f)$$

Prob-value has the advantage that analysis is not restricted to arbitrarily established test levels such as 5% or 10% or to use of standard published tables. The TI 59 Statistics Module has an F distribution program (Program 22) which computes the tail area of an F curve where

the curve is defined by the degrees of freedom in the numerator and the denominator. A series expansion is used to approximate the integral to determine Q(f) [Ref. 10]. If  $H_0$  is true, indicating that all of the observations are from the same normal population, then the prob-value, Q(f), will be large. Conversely, if  $H_0$  is false then the prob-value will be small. If the prob-value is sufficiently small (as determined by the decision-maker) then  $H_0$  is rejected and the conclusion is formed that there must be a difference in the population means somewhere

While a classical test or prob-value may facilitate rejection or acceptance of the null hypothesis, no insight is provided as to which means differ, given that H<sub>0</sub> is rejected. There is an efficient method developed by Sheffe Ref. 13 for computing confidence intervals for the difference between means. If the physical fitness example discussed earlier is used, then Sheffe's development may be used to make the following statements with 95% confidence:

$$(\mu_{i} - \mu_{z}) = (\overline{X}_{i} - \overline{X}_{z}) \pm \sqrt{(r-1)F_{.os}} S_{p} \sqrt{\frac{1}{n_{i}} + \frac{1}{n_{z}}}$$

$$(\mu_{i} - \mu_{3}) = (\overline{X}_{i} - \overline{X}_{3}) \pm \sqrt{(r-1)F_{.os}} S_{p} \sqrt{\frac{1}{n_{i}} + \frac{1}{n_{3}}}$$

$$(\mu_{2} - \mu_{3}) = (\overline{X}_{2} - \overline{X}_{3}) \pm \sqrt{(r-1)F_{.os}} S_{p} \sqrt{\frac{1}{n_{2}} + \frac{1}{n_{3}}}$$

Where  $F_{.05}$  is the critical value of F which leaves 5% in the upper tail,  $S_{\rm p}$  is the square root of the pooled variance, r is the number of means

compared, and n is the size of each of the samples. In the fitness example this equates to making confidence statements about the difference in fitness between the six categories where r is six and n is 6 for each of the samples. To facilitate multiple comparisons a contrast of means is used. This contrast may be written as:

$$\sum C_i \mu_i$$
 where  $\sum C_i = 0$ 

It is then possible to develop the following formula which includes all possible contrasts with 95% confidence:

$$\sum_{i} C_{i} \mu_{i} = \sum_{i} C_{i} \times_{i} \pm \sqrt{(r-i) F_{os}} S_{p} \sqrt{\sum_{i} \left(\frac{C_{i}}{D_{i}}\right)^{2}}$$

If the value 0 is included in a confidence interval then there is no basis for believing that the population means differ while if 0 is not included then the conclusion is drawn that the means do in fact differ.

A program has been developed by Dr. P.W. Zehna Ref. 14 for the TI 59 which computes the elements of an ANOVA table (table B-15)to include the F ratio and prob-value discussed above. Basically the program exploits the TI 59 F distribution program for determining prob-value (Program 22) after using Program 15 of the Statistics Module Ref. 10 to calculate the F statistic. The program then uses Scheffe's multiple contrasts to determine which population means differ given that the null hypothesis is rejected.

A flowchart (figure 5-1), user instructions (table B-13), and a listing of the actual program steps (table B-14) are provided to facilitate description of the ANOVA program. The program takes data input by rows and outputs the elements of an ANOVA table (table B-15) sequentially

as indicated by the number in each block of the table. A row of data constitutes a sample as in the example at table B-16.

The program begins by using Program 06 of the Statistics Module to enter the data. After initialization with 2nd E' each  $x_{ij}$  is entered followed by pressing Label A. When one complete row has been entered a press of 2nd B' causes the calculator to compute the row or sample x and a press of 2nd C' results in computation of the MSD. These two steps must be performed after each row has been input so that the calculator will know when a new row is being entered. When all of the data have been entered using this scheme (table B-13) the sequence RST, A begins the ANOVA Table calculations. The first step under Label A is to call Program 15 of the TI 59 Statistics module which computes the F ratio. In the process of computing the F ratio the other elements of the ANOVA table (table B-15) are computed and stored except for the prob-value. To fill in the values for the ANOVA table all that is required is successive pushes of R/S as indicated in table B-13. For example, the first R/S displays the degrees of freedom for the numerator while the fourth R/S displays the degrees of freedom for the denominator. The program essentially recalls and displays the calculations of Program 15 of the Statistics Module to build the ANOVA table. To compute probvalue the program internally calls Program 22 of the Statistics Module. The user need only press R/S as indicated in table B-13 which causes the calculator to recall the degrees of freedom for the numerator and the denominator used in Pgm 15 and transfer them to Program 22 to define the F Distribution. The F statistic calculated in Program 15 is then

recalled and transferred to Program 22 resulting in  $\Omega(f)$ , the probability that F > f. This prob-value may then be used to accept or reject the null hypothesis. If the null hypothesis is accepted then the analysis is completed. However, if  $H_0$  is rejected, the next step entails the use of Scheffe's contrasts to determine which means differ.

To use the ANOVA program (table B-14) for posterior contrasts with Scheffe's formulas the user initializes the routine by pressing 2nd E'. Then  $c_i$ ,  $x_i$  and  $n_i$  are entered for each row as shown in table B-13. The  $c_i$ 's are the coefficients used to determine which means are contrasted as discussed previously. To contrast  $u_1$  and  $u_2$ ,  $c_1$  = 1,  $c_2$  = -1 and all other  $c_1 = 0$ . To contrast  $u_2$  and  $u_3$ ,  $c_2 = 1$ ,  $c_3 = -1$  and all other  $c_i$  = 0. As these data are input, the program uses a 'loop' to calculate which is stored in register 03 and  $\sum C_i X_i$  which is stored in register 06, (figure 5-1). Register 04 is used as a counter to display the number of row entries. After each  $c_i$ ,  $x_i$  and  $n_i$  entry, register 04 is incremented by one. The program then transfers to Label x2, displays the running count of row entries and stops pending the next entry. After every  $c_i$ ,  $x_i$  and  $n_i$  have been processed, a critical value of F with degrees of freedom r-l and n(r-l) is entered for the desired test level followed by 2nd A'. The program recalls the degrees of freedom for the numerator, r-1, from register 14 and the pooled variance  $S_p^2$  from register 29. The product (r-1)  $F_2$   $S_p^2$  is formed and multiplied by the contents of register 03  $\sum \left(\frac{C_i}{\Gamma_i}\right)$ . The square root of this product is stored in register 05. This value is then added to and subtracted from the contents of register 06,  $\sum c_i x_i$ , to form the desired

confidence interval. The lower bound is displayed after the use of 2nd A' and the upper bound may be recalled by pressing R/S (table B-13).

An example will now be provided using this program to test for differences between population means for the fitness experiments.

### C. APPLICATION OF THE TI 59 ANOVA PROGRAM

The null hypothesis, H<sub>O</sub>, may be stated as - there is no difference in the cardiovascular fitness of those who do no exercise (Category I), those who run in excess of thirty miles per week (Category II), those whose exercise consists solely of lifting weights (Category III), those who lift weights and run in excess of twenty miles per week (Category IV), those who lift weights and run between ten and nineteen miles per week (Category V), and those who do not run or lift weights but participate in other activities such as basketball, racquetball or bicycling (Category VI). Table B-35 reflects the cardiovascular score for each of the thirty-six subjects tested by category as well as the mean for each category. The null hypothesis that there is no difference between these category means may be tested using the ANOVA program with each of the categories constituting a row for input.

After the program card has been read in, the ANOVA program is used by first calling program 06 of the statistics module to enter the data. After initialization with 2nd E', the data for each row are entered followed by A. For the cardiovascular scores (table B-35) the first row, Category I, would be entered as follows: 56.5, A; 58, A; 44.5, A; 33.5, A; 40, A. Once the row data have been entered 2nd B' is pressed to display the row mean, 48.4, followed by C' which displays

the row MSD, 92.9. (The row mean must be recorded for use in posterior contrasts). The data are then entered in a similar fashion for the remaining five rows (Categories II through VI). Once all of the data have been entered, RST is pressed to return the calculator pointer to the ANOVA program. A is then pressed resulting in calculation of the ANOVA Table entries. The ANOVA entries are recalled with sequential presses of R/S. Table B-13 discussed earlier contains detailed instructions on the use of the ANOVA program. Table 5-1 depicts the ANOVA calculations for the cardiovascular scores of the six fitness test categories. The prob-value of .00027 is sufficiently small to cast doubt upon the null hypothesis that there is no difference in the cardiovascular fitness among the six categories tested.

As discussed previously, the prob-value tells how credible the null hypothesis is but it does not tell which categories differ given that there is cause to reject  $H_0$ . However, confidence intervals may be established for contrasts between the categories using Scheffe's formula which is programmed in the ANOVA routine  $\begin{bmatrix} Ref. & 13 \end{bmatrix}$ . For the cardiovascular example, the cardiovascular fitness of the sedentary subjects (Category I) may be contrasted to the cardiovascular fitness of the runner (Category II) as a demonstration of the program. 2nd E' is pressed to initialize the contrast routine followed by  $c_i$ ,  $x_i$  and  $n_i$  for each of the two rows. For Categories I and II the entries are:

<sup>1</sup> R/S 48.4 R/S 6 R/S

<sup>-1</sup> R/S 83.4 R/S 6 R/S

The appropriate F percentile is entered followed by A' to generate the desired confidence interval. To display a 95% confidence interval for the difference in cardiovascular fitness between Categories I and II an F percentile of 2.53 (where there are five degrees of freedom in the numerator and thirty degrees of freedom in the denominator) is used resulting in an interval from -65.5 to -41.4. Since 0 is not included in the interval it is reasonable to conclude that there is a difference in the cardiovascular fitness of the two categories. Table 5-2 contains the results of contrasting each of the six fitness categories. Only four contrasts result in the conclusion that there is a difference between the categories with 95% confidence: Category I - Category II (-65.5, -41.4); Category I - Category IV (-65.5, -4.4); Category II -Category III (.6, 61.8) and Category III - Category IV (-61.7, -6.0). These results indicate with 95% confidence that there is a difference in the cardiovascular fitness of those who run more than twenty miles per week (Categories II and IV) and those who do no running at all (Categories I and III), at least for those subjects examined.

The ANOVA program has also been applied to the strength and cardiovascular scores resulting from the experiment. Table B-36, Appendix B, reflects the strength scores of each of the thirty-six subjects by category. The ANOVA results are contained in Table 5-3. The prob-value of .12 x 10<sup>-8</sup> indicates that the null hypothesis that there is no difference in the strength of members of the different categories should be rejected. Further analysis with posterior contrasts is necessary to see which categories differ. Table 5-4 contains the results of posterior contrasts with an F percentile of 2.53 for 95%

confidence with five and thirty degrees of freedom for the numerator and denominator respectively. Unlike the cardiovascular contrasts there are a number of differences in the strength results. Categories III and IV, which were composed of the most ardent weightlifters, differs from Categories I and III but not VI. These results are not surprising in that they confirm the hypothesis that different training programs result in different levels of fitness. In this instance where fitness is defined as strength, those who trained for strength were in fact stronger than those who did not. Again, without attempting inference to a larger population, these results may be used to gain insight into the probable differences that might be tested in a more appropriately designed experiment.

Table B-37, Appendix B depicts the endurance scores for the thirty-six subjects by category. Table 5-5 reflects the results of using the ANOVA program with the endurance scores as input. Once again, the prob-value of .137 x 10<sup>-6</sup> indicates rejection of the null hypothesis (in this case that there is no difference in the upper body endurance of the members of the six different categories). The posterior contrasts (table 5-6) indicate that the weightlifters (Categories III, IV, V) differ from the non-weightlifters (Categories I, II, VI) in upper body endurance with 95% confidence. This also supports the hypothesis that different training programs result in different levels of fitness, subject again to the sampling restrictions previously discussed.

## D. SUMMARY

While the results of the fitness experiment are interesting, the purpose of this analysis has been to demonstrate a statistical application of the TI 59 and not draw inference to a hitherto undefined population. The univariate program was used to calculate measures of central tendency and spread for the Category I Cardiovascular scores. The ANOVA program was used to test for differences in strength, endurance, and cardiovascular fitness among the six test categories. In both instances meaningful but guarded inferences were drawn from the test data.

The capabilities of the TI 59 in real world statistical analysis are impressive. The analyst can conduct sophisticated analysis of good-sized samples unconstrained by access to large computers. Using programs such as those demonstrated in this chapter the analyst need not even learn a programming language. All that is required to compute an F ratio or prob-value, for example, is the ability to follow simple users' instructions. While there are certainly samples whose size preclude the use of the TI 59, there are a pletheora of samples which can be analyzed more conveniently and just as efficiently at home or at the office using the TI 59.

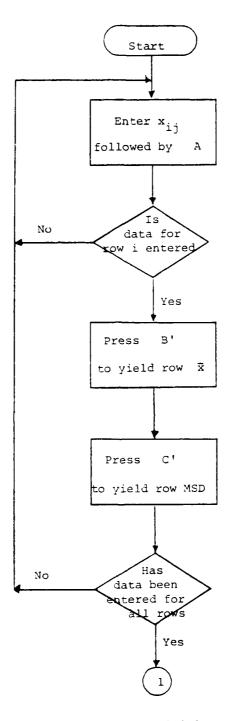


Figure 5-1.1

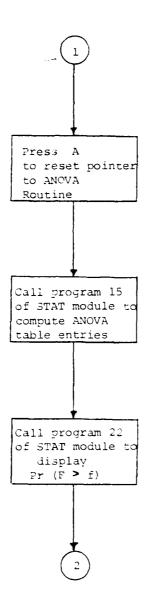


Figure 5-1.2

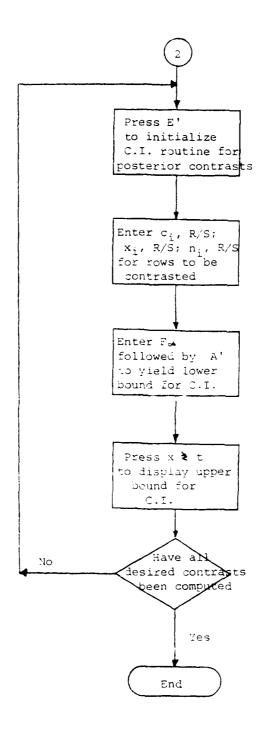
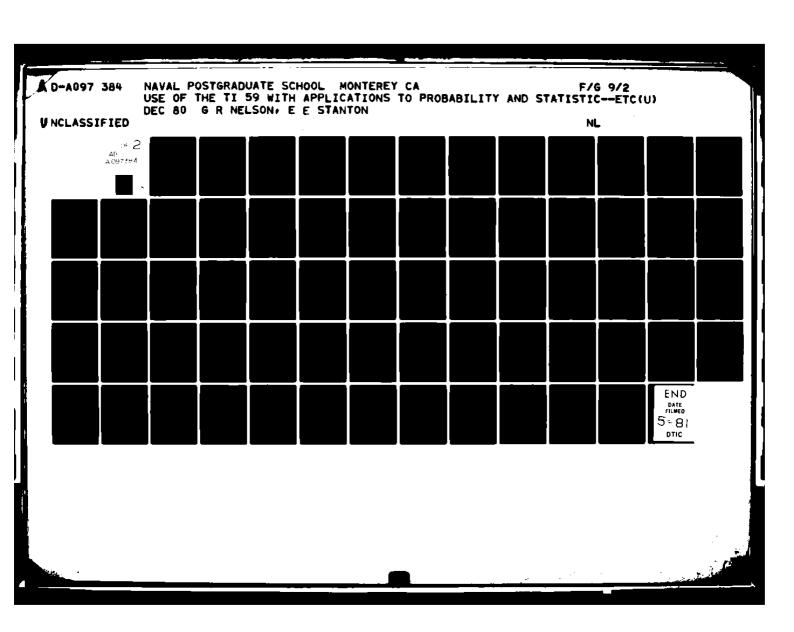


Figure 5-1.3



## SUM OF SQUARES

## DECREES OF FREEDOM

## VARIANCE

## F RATIO

$$\begin{array}{ccc} & r & \\ n & \sum & (\bar{x}_1 - \bar{x})^2 \\ & & \\ & & \end{array}$$

3 1478.3

(2) 5.00

① 7391.6

$$\begin{array}{ccc} r & n \\ \Sigma & \Sigma & (x_{1j} - \bar{x}_1)^2 & r(n-1) \\ 1 & j & \end{array}$$

5 30.0

0.0999 (4)

 $^{8}_{\rm p}$ 

TOTAL 
$$\Sigma$$
  $\Sigma$  ( $\mathbf{x_{1,j}}$ 

$$\begin{array}{ccc}
\Sigma & \Sigma & (x_{1j} - \bar{x})^2 & (nr - 1) \\
1 & j & \end{array}$$

TABLE 5-1

# CARDIOVASCULAR CONTRASTS

| 9   | -53.1          | -18.1<br>43.1 | -49.2<br>11.9  | -18.1<br>43.1 | -45.7<br>15.5 |  |
|-----|----------------|---------------|----------------|---------------|---------------|--|
| ٧   | -37.9<br>23.2  | - 2.9         | -34.2          | - 2.9         |               |  |
| 7   | - 4.4          | -30.6<br>30.6 | -61.7<br>- 6.0 |               |               |  |
| 3   | -34.3<br>26.7  | .6<br>61.8    |                |               |               |  |
| ત્ય | -65.5<br>-41.4 |               |                |               |               |  |
| 1   |                |               |                |               |               |  |
|     |                |               |                |               |               |  |

N

| SOURCE OF   | S |
|-------------|---|
| UADT ABTA   | 1 |
| VARLATION V | S |
|             | ֡ |

PROB-VALUE

(r - 1)

BETWEEN ROWS

(2) 5.00

1) 7.98

 $\begin{array}{ccc} \mathbf{r} & \mathbf{n} \\ \Sigma & \Sigma \\ \mathbf{1} & \mathbf{j} & (\mathbf{x_{1j}} - \bar{\mathbf{x_{1}}})^2 & \mathbf{r(n-1)} \end{array}$ 

WITHIN ROWS

S 30.00

(t) 1.99

$$\begin{array}{ccc} \Sigma & \Sigma & (\mathbf{x_{1j}} - \bar{\mathbf{x}})^2 & (nr - 1) \\ 1 & \mathbf{j} & \end{array}$$

TOTAL

TABLE 5-3 .

## STRENGTH CONTRASTS

| 9           | 72<br>46.    | - 58         | .50 | .34       | 06 |  |
|-------------|--------------|--------------|-----|-----------|----|--|
| 2           | - 1.19       | - 1.05       | .03 | 13<br>.93 |    |  |
| †           | - 1.59       | - 1.45       | 37  |           |    |  |
| 8           | - 1.75<br>69 | - 1.61<br>55 |     |           |    |  |
| 83          | 67           |              |     |           |    |  |
| <del></del> |              |              |     |           |    |  |
|             |              |              |     |           |    |  |

99

## ENDURANCE ANOVA TABLE

| VARIANCE   |           |
|------------|-----------|
| DEGREES OF | FREEDOM   |
| SUM OF     | SQUARES   |
| SOURCE OF  | VARIATION |

PROB-VALUE

F RATIO

nS2 x

(r-1)

BETWEEN ROWS

(3) 1329.92

(1) 6649.64 (2) 5.00

(10) 
$$.137 \times 10^{-6}$$

TOTAL 
$$\sum_{i} \sum_{j} (x_{i,j} - \bar{x})^2$$
 (nr - 1)

$$(nr - 1)$$

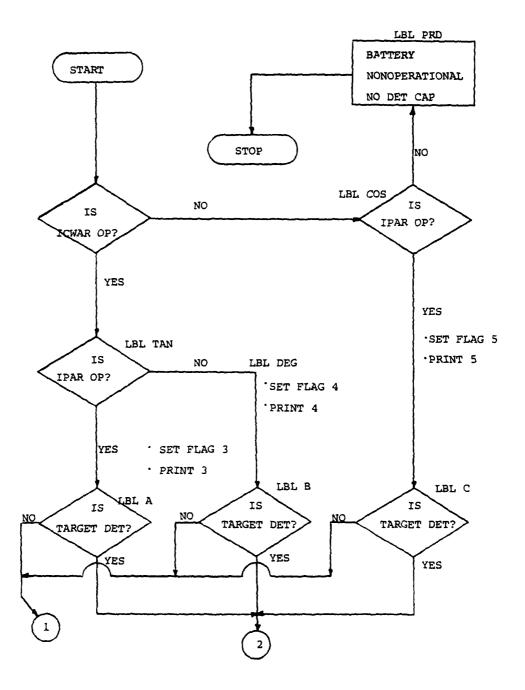
| 9        | -20.31<br>17.55  | -20.59<br>17.26  | 10.90<br>48.76  | 8.82<br>46.68   | - 1.24<br>36.61 |  |
|----------|------------------|------------------|-----------------|-----------------|-----------------|--|
| 5        | -37.99           | -38.29           | - 6.79<br>31.06 | - 8.87<br>28.99 |                 |  |
| 7        | -48.06<br>-10.20 | -48.35<br>-10.49 | -16.85<br>21.00 |                 |                 |  |
| <b>س</b> | -50.14<br>-12.28 | -50.43<br>-12.57 |                 |                 |                 |  |
| 8        | -18.64<br>19.22  |                  |                 |                 |                 |  |
| 1        |                  |                  |                 |                 |                 |  |
|          |                  |                  |                 |                 |                 |  |

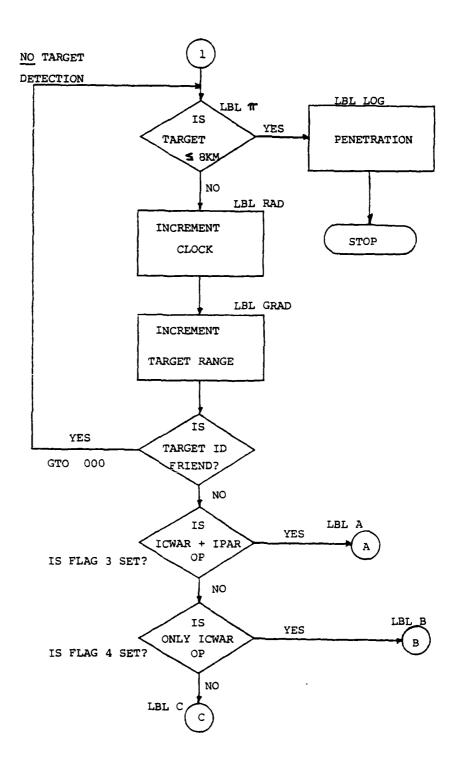
## APPENDIX A

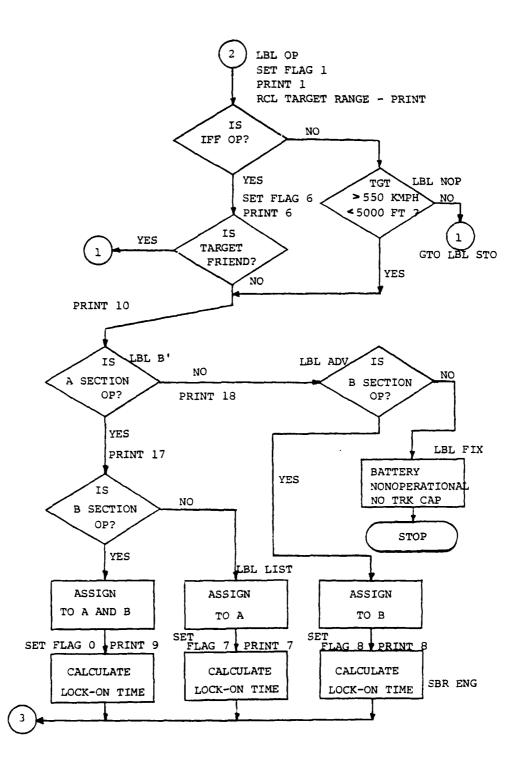
## COMMENTS ON SELECTED LABELS

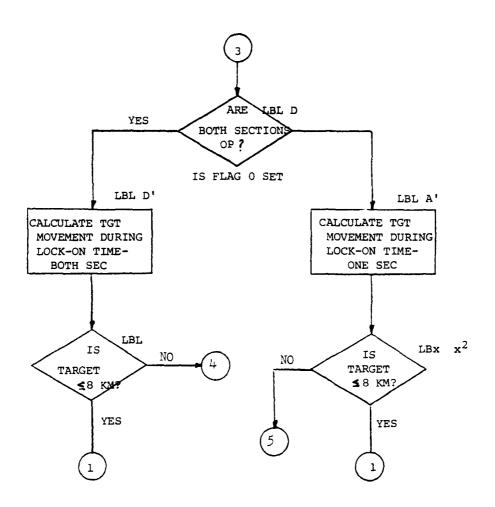
| LABEL                   | COMMENT  |
|-------------------------|--|
| A                       | Directs action to compute glimpse probability of detection for both ICWAR and IPAR                         |
| x                       | Computes glimpse probability of detection for ICWAR only based on target range                             |
| $\overline{\mathbf{x}}$ | Computes glimpse probability of detection for IPAR only based on target range                              |
| E and LnX               | Determines if target is less than 40 KM from unit and directs processing accordingly.                      |
| ים'                     | Calculates target range after elapse of target lock-on time.   |
| (SBR) EXC a             | nd INT Increments range of IHAWK missile after firing  |
| FIX                     | Prints 24 (no firing capability)   |
| DSZ                     | Prints 14 (cruise missile identified as friend)  |
| NOP                     | Prints 66 (IFF is nonoperational)  |
| OP                      | Prints 1 (target detected) at range (KM), begins engagement sequence                                       |
| (SBR) RAD a             | nd $y^x$ Increments simulated air battle time clock $(R_{19})$ .   |
| (SBR) GRAD              | and $\frac{1}{X}$ Computes cruise missile rate of approach and increments target range (R <sub>00</sub> ). |
| (SBR) ENG               | Random number generation - normal distribution   |
| (SBR) P→R               | Random number generator - uniform distribution   |
| PRD                     | Prints 23 (no detection capability)  |
| SIN                     | Prints "KILL" and range of target kill   |
| LOG                     | Prints "PENETRATION"   |
| (SBR) WRITE             | AND $\pi$ Prints "PENETRATION" if target is 8 KM or less   |

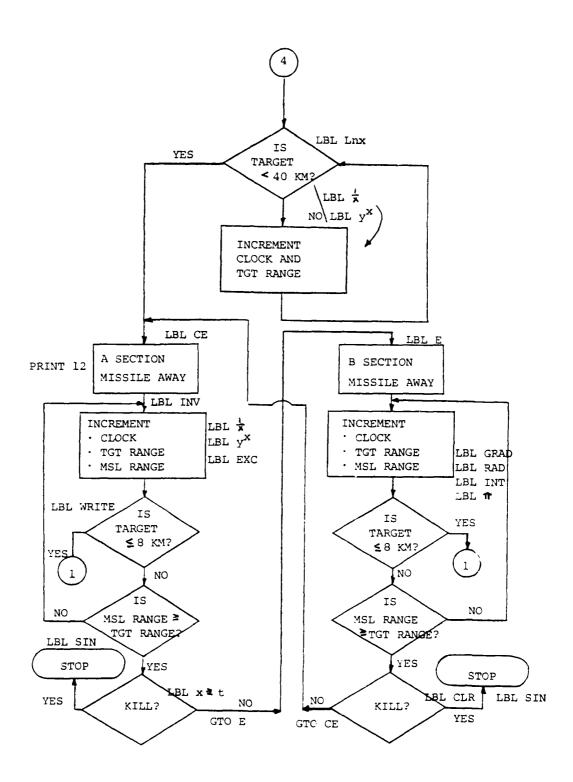
from unit.

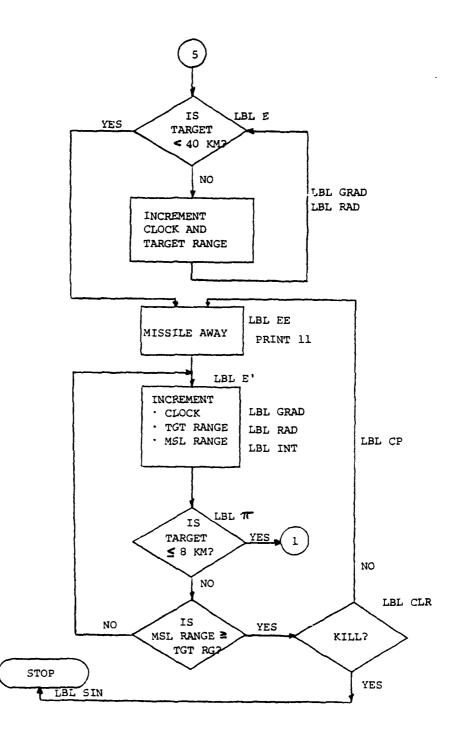












# SIMULATION PROGRAM

|   |   | *  |   |   |
|---|---|--|---|---|
| 000<br>001<br>002<br>003<br>004<br>005<br>006<br>007<br>008<br>010<br>011               | 71 SBR<br>89 . 1<br>71 SBR<br>80 GRD<br>71 SBR<br>70 RAD<br>87 IFF<br>02 02<br>00 00<br>87 IFF<br>03 03<br>11 A   |  | 041<br>042<br>043<br>044<br>045<br>047<br>048<br>051<br>051<br>053<br>054 | 05 5<br>99 PRT<br>13 C<br>76 LBL<br>30 TAN<br>71 SBR<br>37 P/R<br>93 .<br>09 9<br>05 5<br>32 X:T<br>77 GE<br>60 DEG<br>86 STF         |
| 013<br>014<br>015<br>016<br>017<br>018<br>020<br>021<br>022<br>023                      | 87 IFF<br>04 04<br>12 B<br>87 IFF<br>05 05<br>13 C<br>71 SBR<br>37 P/R<br>93 .<br>06 6<br>05 5<br>32 X:T<br>77 GE | :  | 055<br>056<br>057<br>059<br>060<br>061<br>063<br>064<br>065               | 03 03<br>99 PRT<br>11 A<br>76 LBL<br>60 DEG<br>86 STF<br>04 04<br>04 4<br>99 PRT<br>12 B<br>76 LBL                                    |
| 025<br>026<br>026<br>027<br>029<br>030<br>033<br>033<br>033<br>033<br>038<br>039<br>040 | 77 GE<br>39 COS<br>61 GTON<br>76 LBL<br>39 COS<br>71 SBR<br>93 9<br>05 X GE<br>905 X GE<br>905 STF<br>905 OS      | is - combined to the party of the control of the co | 067<br>068<br>070<br>071<br>072<br>073<br>075<br>076<br>078<br>081        | 69 □P<br>01 1<br>99 PRT<br>43 RCL<br>00 00<br>99 PRT<br>71 SBR<br>37 P/R<br>93 .<br>09 9<br>05 5<br>32 X↓T<br>77 GE<br>68 N□P<br>06 6 |

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# APPENDIX B INSTRUCTION SHEET

This is a physical fitness test.

#### I. WHAT WE ARE EXAMINING AND WHY

The following tests will look at the complex systems that make up the network of health and fitness. First we will test your upper body endurance and muscular strength. Next we will examine your cardiovascular health. This test is a component of a research project being conducted by graduate students of the Naval Postgraduate School.

#### II. MUSCULAR ENDURANCE AND STRENGTH

Muscular endurance is often synonymously and incorrectly used in place of muscular strength. Muscular strength is the ability of your muscular system to exert maximum force against an object or resistance all at once, your ability to exert a maximum force a single time.

Muscular endurance relates to the ability to exert force, not necessarily maximal, over an extended time period. As with all the components of fitness, these two concepts are interrelated but distinctly different from each other. Each concerns itself with particular capacities of fitness.

#### III. CARDIOVASCULAR HEALTH

Objective: To measure your heart-rate response to exercise. This test will determine the relative efficiency of your heart and circulatory system. Your heart rate can be used to describe the fitness level of your body in three areas: how much oxygen you need, how much blood

TABLE B-1.1

your heart must pump to supply this need, and how hard your heart must work at this task. If your need for oxygen is not being fulfilled, your body is working in an inefficient manner. Consequently, more blood will have to be pumped through your circulatory system at a faster rate to get the oxygen to the muscles and organs that need it. The heart has the responsibility of satisfying your body's need for oxygen. It will have to beat more frequently to circulate the blood throughout your system. If your body works in an efficient manner, its need for oxygen is being fulfilled.

Thus cardiovascular health relates to the ability of the heart, lungs, and blood vessels to work in unison without strain. Regardless of what the task is, whether physical or mental, the cardiovascular system should be able to handle it. When you have high levels of cardiovascular health you perform with more efficiency and you are more effective at what you do.

#### QUESTIONNA IRE

# THIS IS A PHYSICAL FITNESS TEST READ THIS DOCUMENT CAREFULLY BEFORE THIS TEST BEGINS

- (1) This test is completely voluntary! You may decline testing now if you wish. You may stop at any time during this test and decline further testing. You are under no obligation to complete this test.
- (2) Before proceeding with this test, you should assure yourself and your tester that there have been no incidents in your medical history that would prohibit you from pursuing this testing. Your medical history is relevant to this physical fitness test.
- (3) Please answer the following statements: YES or NO
  - (a) I have a heart related disease.
  - (b) I have high blood pressure.
  - (c) I often feel faint and suffer spells of dizziness.
  - (d) I have recently or in the past felt pain, heaviness or pressure in my chest.
  - (e) I have felt pain, heaviness or pressure in my chest when I walk uphill.
  - (f) My doctor has advised me not to engage in physical exercise or physical activity.
- (4) I have read and fully understand this document.

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# DATA SHEET

| NAME                 |                      |        |             | <del></del> |       |               |             |
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| AGE                  | WEIGHT               |        | <del></del> | DATE        |       | -             |             |
| PHYSICAL ACTIVITY CA | TEGORY:              | I      | II          | III         | IA    | Λ             | VI          |
| STRENGTH TEST:       | Maximu               | m Beno | ch Pre      | ess         |       |               |             |
|                      | Maximu               | m Cur  | L           |             |       |               |             |
| ENDURANCE TEST:      | Ben <b>ch</b> 1      | Press  | Repet       | itions W    | ith 1 | .00 Pc        | ounds       |
|                      | Curl R               | epeti  | tions       | With 55     | Pound | ls            |             |
| CARDIOVASCULAR TEST: | : (Pulse :<br>Restin |        |             |             |       |               |             |
|                      | Immedi               | ate Po | ost Ex      | ercise      |       |               |             |
|                      | 30 Sec               | onds 1 | Post E      | xercise     |       | <del></del> - | <del></del> |
|                      | 60 Sec               | onds 1 | Post E      | xercise     |       |               |             |
|                      | 120 Se               | conds  | Post        | Exercise    | ,     |               |             |

|                                    |          |     |    |    |    |  |     |     |     | Codes    | Sa   |     |            |     |     |  |      |     |      |                  |       |
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| Resting<br>Heart Rate              | 4        | 43  | 52 | 56 | 8  | 62   | 2   | 99  | 8   | 20       | 22   | 74  | 92.        | 78  | 80  | 꿃                                      | 88   | 92  | 96   | 96 100           |       |
| Posttest<br>Heart Rate             | 8        | ಷ   | 88 | 92 | %  | 96 100 104 108 112 116 120 124 128 132 136 140 144 148 | 104 | 108 | 112 | 116      | 120  | 124 | 128        | 132 | 136 | 140                                    | 144  | 148 | 152  | . 152 156        |       |
| Second<br>Recovery<br>Heart Rate   | 2        | 3   | 8  | 92 | 8  | 2  | 88  | 8   | %   | <u> </u> | 96 100 104 108 112 116 120 124 128 132 136 140 | 108 | 112        | 116 | 120 | 124                                    | 128  | 132 | 136  | 140              |       |
| 1 Minute<br>Recovery<br>Heart Rate | 28       | . 8 | 2  | 89 | 8  | 92   | 80  | 84  | 88  | 22       |  | 18  | 96 100 104 |     | 112 | 108 112 116 120 124                    | 120  |     | 128  | 132              |       |
| 2 Minute<br>Recovery<br>Heart Rate | <u> </u> | 99  | 2  | જ  | 2  | 92   | 80  | 2   | 88  | 92       |  | 100 | 104        | 138 | 112 | 96 100 104 108 112 116 120 124 128 132 | 120  | 124 | 128  | 132              |       |
|                                    |          |     |    |    |    |  |     | 1   |     |          |  |     |            |     |     | ] [                                    | otal | ع [ | de S | Total Code Score |       |

TABLE B-4

#### CATEGORY I RESULTS

| SUBJECT | ACE | WEIGHT      | CARDIOVASCULAR<br>SCORE (1) | STRENCTH<br>SCORE (2) | ENDURANCE<br>SCORE (3) |
|---------|-----|-------------|-----------------------------|-----------------------|------------------------|
| 1       | 29  | 190         | 56.5                        | 1.26                  | 24.1                   |
| 2       | 33  | 155         | 58.0                        | 1.32                  | 12.9                   |
| 3       | 36  | 170         | 58.0                        | •97                   | 5.5                    |
| 4       | 31  | 205         | 44.5                        | 1.19                  | 27.9                   |
| 5       | 37  | <b>1</b> 57 | 33.5                        | 1.13                  | 10.1                   |
| 6       | 34  | 160         | 40.0                        | 1.16                  | 11.0                   |

<sup>(1)</sup> See Table B-17 for derivation(2) See Table B-18 for derivation(3) See Table B-19 for derivation

# CATECORY II RESULTS

| SUBJECT | AGE | WEIGHT | CARDIOVASCULAR<br>SCORE (1) | STRENGTH<br>SCORE (2) | ENDURANCE<br>SCORE (3) |
|---------|-----|--------|-----------------------------|-----------------------|------------------------|
| 1       | 33  | 167    | 91.5                        | 1.47                  | 22.0                   |
| 2       | 34  | 195    | 96.5                        | 1.41                  | 28.9                   |
| 3       | 35  | 180    | 55.0                        | 1.11                  | 12.2                   |
| 4       | 33  | 160    | 93•5                        | 1.44                  | 13.6                   |
| 5       | 28  | 127    | 82.0                        | 1.34                  | 6.5                    |
| 6       | 30  | 158    | 82.0                        | 1.11                  | 6.6                    |

See Table B-20 for derivation
 See Table B-21 for derivation
 See Table B-22 for derivation

# CATEGORY III RESULTS

| SUBJECT | AGE | WEIGHT | CARDIOVASCULAR<br>SCORE (1) | STRENGTH<br>SCORE (2) | ENDURANCE<br>SCORE (3) |
|---------|-----|--------|-----------------------------|-----------------------|------------------------|
| 1       | 22  | 200    | 35.0                        | 2.48                  | 50.0                   |
| 2       | 23  | 202    | 56.0                        | 2.35                  | 62.5                   |
| 3       | 28  | 205    | 44.5                        | 2.49                  | 37.2                   |
| 4       | 34  | 220    | 86.5                        | 2.23                  | 42.7                   |
| 5       | 25  | 180    | 67.0                        | 2.83                  | <b>54.</b> 8           |
| 6       | 29  | 225    | 24.5                        | 2.00                  | 1.6                    |

See Table B-23 for derivation
 See Table B-24 for derivation
 See Table B-25 for derivation

# CATEGORY IV RESULTS

| SUBJECT | AGE       | WEICHT      | CARDIOVASCULAR<br>SCORE (1) | STRENCTH<br>SCORE (2) | ENDURANCE<br>SCORE (3) |
|---------|-----------|-------------|-----------------------------|-----------------------|------------------------|
| 1       | 28        | 200         | 96.5                        | 2.30                  | 47.5                   |
| 2       | 31        | 180         | 79.0                        | 2.67                  | 49.0                   |
| 3       | 32        | <b>1</b> 65 | 85.0                        | 2.00                  | 43.7                   |
| 4       | <b>32</b> | <b>1</b> 60 | 79.0                        | 2.19                  | 47.2                   |
| 5       | 19        | 240         | 89.5                        | 1.85                  | 34.3                   |
| 6       | 26        | 180         | 71.5                        | 2.39                  | 44.6                   |

See Table B-26 for derivation
 See Table B-27 for derivation
 See Table B-28 for derivation

# CATEGORY V RESULTS

| SUBJECT | AGE | WEIGHT | CARDIOVASCULAR<br>SCORE (1) | STRENCTH<br>SCORE (2) | ENDURANCE<br>SCORE (3) |
|---------|-----|--------|-----------------------------|-----------------------|------------------------|
| 1       | 30  | 165    | 39•5                        | 2.03                  | 25.5                   |
| 2       | 24  | 175    | 55.0                        | 2.43                  | 54.1                   |
| 3       | 19  | 185    | 47.0                        | 1.86                  | 47.0                   |
| ü       | 34  | 179    | 77.5                        | 1.73                  | 33.5                   |
| 5       | 35  | 205    | 59•5                        | 1.15                  | 22.0                   |
| 6       | 30  | 120    | 56.5                        | 1.75                  | 23.8                   |

See Table B-29 for derivation
 See Table B-30 for derivation
 See Table B-31 for derivation

# CATEGORY VI RESULTS

| SUBJECT | ACE | WEIGHT | CARDIOVASCULAR<br>SCORE (1) | STRENGTH<br>SCORE (2) | ENDURANCE<br>SCORE (3) |
|---------|-----|--------|-----------------------------|-----------------------|------------------------|
| 1       | 27  | 180    | 61.0                        | 1.42                  | 23.1                   |
| 2       | 32  | 125    | 47.5                        | 1.56                  | 17.4                   |
| 3       | 31  | 170    | 65.5                        | 1.26                  | 14.7                   |
| 4       | 31  | 170    | 85.0                        | 1.41                  | 15.3                   |
| 5       | 33  | 175    | 86.5                        | 1.34                  | 11.4                   |
| ó       | 30  | 205    | 30.0                        | 1.15                  | 17.9                   |

<sup>(1)</sup> See Table B-32 for derivation (2) See Table B-33 for derivation (3, See Table B-34 for derivation

|      | Univariate Use         | Instructio | ns            |                       |
|------|------------------------|------------|---------------|-----------------------|
| Step | Procedure              | Enter      | Press         | Display               |
| 1.   | Initialize             |            | 2nd E'        | 31                    |
| 2.   | Enter data             | ×i         | A             | i                     |
|      | Repeat for each x      |            |               |                       |
| 3.   | Recall Statistics      |            | 2nd ₹         | x                     |
|      |                        |            | INV 2nd R     | s                     |
| {    |                        |            | 2nd OP 11     | MSD                   |
|      |                        |            | RCL 12        | x <sub>min</sub>      |
| {    |                        |            | RCL 13        | x <sub>max</sub>      |
|      |                        |            | RCL 14        | MIDVAL                |
|      |                        |            | RCL 15        | range                 |
|      |                        |            | 2nd A'        | MAD                   |
|      |                        |            | RCL 03        | n                     |
| 4.   | Recall data entered in |            | İ             |                       |
|      | Step 2 if desired.     |            | RCL 31        | ×ı                    |
|      |                        |            | RCL 32        | <b>x</b> <sub>2</sub> |
|      |                        |            | RCL 31 + i -1 | *i                    |
|      |                        |            |               |                       |
|      |                        |            |               |                       |
|      |                        |            |               |                       |
|      |                        |            |               |                       |
|      |                        |            | 1             |                       |

TABLE B-11

# UNIVARIATE PROGRAM

```
000
     76 LBL
                                     C.
                            041
                                  18
      10 E'
001
                                  22 INV
                            042
     47 CMS
002
                            043
                                  77
                                       GE
003
     22 INV
                            044
                                  00
                                       00
004
     86 STF
                            045
                                  57
                                      57
005
     00 00
                            046
                                  43 RCL
     03 3
006
                            047
                                  13
                                      13
007
      01
         1
                            048
                                  32 X:T
      42 STO
008
                            049
                                  43 RCL
009
      30 30
                            050
                                  18
                                      18
     91 R/S
010
                            051
                                  77
                                      GΕ
     76 LBL
011
                            052
                                  00
                                      00
012
     11
         Ħ
                            053
                                  62
                                       62
013
     42 STO
                            054
                                  61 GTO
014
     18
         18
                            055
                                  00
                                      0.0
015
      72 ST*
                            056
                                  64
                                      64
016
      30 30
                            057
                                  42 STD
017
      01
         1
                                  12
                            058
                                     12
018
      44 SUM
                            059
                                  61 GTD
019
      30 30
                            060
                                  00 00
020
     87 IFF
                            061
                                  64 64
     00 00
65 ×
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                            062
                                  42 STD
022
023
                            063
                                  13 13
      43 RCL
                                  53 (
53 (
                            064
024
      18 18
                            065
025
      42 STD
                            066
                                  43 ROL
026
      12 12
                                 12 12
85 +
                            067
026
027
028
029
030
031
      42 STD
                            068
      13 13
                                 43 RCL
13 13
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     78 Σ+
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     86 STF
                            071
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      00
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073
                                  55
      43 RCL
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033
      03
        03
                            074
                                  54
034
      91 R/S
                            075
                                  42 STD
      76 LBL
035
                            076
                                  14 14
036
      65 ×
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                                 53
                                     ŧ
      43 RCL
037
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                                  43 ROL
     12 12
32 X:T
038
                            079
                                  13 13
039
                            080
                                     _
     43 RCL
040
                            081
                                  43 ROL
```

TABLE B-12.1

```
082
083
084
        12
                                      124
                                              07
        54
                                      125
126
127
128
129
130
131
135
136
137
138
139
                                                   SUN
                                              44
        42
                                              43
                                                   43
085
086
087
088
089
        15
             15
                                                   D ÷
                                              19
        43
            RCL
                                              55
43
        18
             13
                                                   ROL
            GTO
        61
                                              03
                                                   -03
        00
              00
                                              95
                                                    =
        29
76
090
              29
                                              91
                                                   R/S
091
092
093
           LBL
                                              76
                                                  LBL
        16 A'
                                                    D
3
                                              14
                                              03
        94 +2- 1
094
                                              01
                                                    1
        42
16
095
            STO
                                              42
                                                   STD
096
             16
                                              30
                                                   30
        43 RCL
03 03
097
                                              91
                                                   R/S
098
                                      140
                                              00
                                                    Ü
099
100
        42 STD
                                              00
                                      141
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        07
              07
                                      14234454478491450145567891601
                                              00
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101
102
              3
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                                              0 \, 0
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        01
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103
        42 STB.
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            20
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105
        00
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                                              00
                                                    Ū
106
        42 STD
                                              00
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107
        19-119
                                              00
                                                    Ð
108
        76 LBL
                                              00
                                                    0
109
        44
            SUM
                                              00
                                                    O
110
111
112
113
        53
              (
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                                                    0
        73
            RC*
                                              00
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              20
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        85
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114
        43 RCL
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115
        16
              16
                                              00
116
117
        54
              >
                                              00
        50; I×I
                                              00
113
        44
             SUM
                                              00
                                                    0
119
120
121
122
        19
              19
                                              00
                                                    0
        01
              1
                                      162
                                              00
                                                    0
        44
             SUM
                                      163
                                              00
                                                     Ó
              20
        20
```

TABLE B-12.2

|          | anova user in   | STRUCTIONS      |            |                      |
|----------|---|-----------------|------------|----------------------|
| Step     | Procedure   | Enter           | Press      | Display              |
| 1        | Select Program 06   |                 | 2nd Pgm 06 |                      |
| 2        | Initialize data base                                      |                 | 2nd E'     | 0                    |
| 3        | Enter data for each row                                   | × <sub>ij</sub> | A          | ri                   |
| i,       | Reset pointer if more<br>than 29 data entries<br>are made |                 | ם          | 31                   |
| 5        | Calculate x for current                                   |                 | 2nd B'     | x <sub>i</sub>       |
| 6        | Calculate MSD for current row                             |                 | 2nd C'     | MSD <sub>i</sub>     |
| 7        | Return to step 3 to enter next row data                   |                 |            |                      |
| 8        | Return pointer to<br>ANOVA program                        |                 | RST        |                      |
| 9        | Calculate ANOVA table entries Note: the numbers in        |                 | A          | ss <sub>r</sub> (1)  |
| <u> </u> | parentheses in the display column                         |                 | R/S        | r-1 (2)              |
|          | correspond to the numbered blocks in                      |                 | R/S        | $MSS_{r}$ (3)        |
|          | the ANOVA table (table 4-4)                               |                 | R/S        | SS <sub>u</sub> (4)  |
|          |   |                 | R/S        | r(n-1) (5)           |
|          |   | "               | R/S        | MSS <sub>u</sub> (6) |
|          |   |                 | R/S        | ss <sub>t</sub> (7)  |
|          |   |                 | R/S        | (nr-1) (8)           |
|          |   |                 | R/S        | F ratio (9)          |
|          |   |                 | R/S        | Prob-value (10)      |

TABLE B-13.1

|      | ANOVA USER   | INSTRUCTIONS   |             |                |
|------|--|----------------|-------------|----------------|
| Step | Procedure  | Enter          | Press       | Display        |
|      | Confidence Intervals fo                                | r              |             |                |
| 10   | Initialize   |                | E *         | 0              |
| 11   | Enter contrast data                                    | c <sub>i</sub> | R/S         | c <sub>i</sub> |
|      | Repeat for each row i                                  | ×i             | R/S         | ×i             |
|      |  | n <sub>i</sub> | R/S         | n <sub>i</sub> |
| 12   | Enter F percentile with degrees of freedom r-1, r(n-1) | F              | A'<br>x ₹ t | l<br>µ         |
|      |  |                |             |                |

TABLE B-13.2

#### ANOVA PROGRAM

```
032
     76 LEL
ODO
                                       1
                                  01
                             033
     11 A
001
                                   95
                             034
     36 PGM
002
                                      R/S
                             035
                                   91
         15
      1.5
0u3
                                   43 RCL
                             036
         A
004
      11
                                      00
                                   00
                             037
      42 STD
005
                                   91 R/S
                             038
         00
      00
006
                                   43 ROL
                             039
      43 RCL
007
                             040
                                   14
                                       14
         08
      80
008
                                   36 PGM
                             041
      91 R/S
009
                                   22
                                       22
                             042
      43 RCL
010
                                       A
                                   11
                             043
         14
      14
011
                                   43 RCL
                             044
      91 R/S
012
                                       16
                             045
                                   16
      43 RCL
013
                             046
047
                                      PGM
                                   36
         15
      15
 014
                                       22
                                   22
      91 R/S
 015
                                   12
                                       Β
                             048
      43 RCL
 016
                                   43 RCL
                             049
          13
 017
      13
                                       00
                             050
                                   00
       91 R/S
 018
                                    36 PGM
                             051
       43 RCL
 019
                                       22
C
                             052
050
                                    22
          16
       16
 020
                                    13
       91 R/S
                                   92 RTM
76 LBL
 021
                              054
       43 RCL
 022
                              055
           17
       17
 023
                                    10 E'
                              056
       42
          STO
 024
025
                                    36 PGM
                              057
058
       29
           29
                                        01
                                    Ū1
       91 R/S
 026
                              059
                                    71 SBR
       43 RCL
 027
                                    25 CLR
76 LBL
                              060
       12
           12
 023
                              061
       91 R/S
 029
                                    33 X2
                              062
       43 RCL
  U30
                                    91 R/S
                              063
      ., 09
            09,.....
031
```

```
064
                                095
      42 STD
                                      65
065
      01
          01
                                      43 RCL
                                096
066
067
      91 R/S
                                097
                                      14
                                          14
      42 STO
                                098
                                      65
                                           \times
068
                                      43 RCL
      02
          02
                                099
069
070
071
072
073
074
075
076
      91 R/S
                                100
                                      29
                                           29
      35 1/X
                                101
                                      65
                                           X
      65
          ×
                                102
                                      43 RCL
      43 RCL
                                103
                                      03
                                          03
      01
          01
                                104
                                      95
                                           =
                                      34 IX
      33 X2
                                105
      95
                                      42 STO
          =
                                106
      44
          SUM
                                107
                                      05
                                          05
      03
         -03
                                108
                                      85
                                          +
078
      43 RCL
                                109
                                      43 RCL
079
      01
          01
                                110
                                      06
                                          06
080
      65
          \times
                                111
                                      35
                                112
113
                                      32 X:T
081
      43 RCL
082
      02
          02
                                      43 RCL
      95
083
          =
                                114
                                      06
                                          -06
084
      44
          SUM
                                115
                                      75
                                          _
085
      06
          06
                               116
                                      43 ROL
086
                               117
      01
          1
                                      05
                                         05
087
      44 SUM
                               118
                                      95
                                          =
088
      04
          0^{A}
                               119
                                      92 RTN
089
                               120
      43 RCL
                                      00
                                          0
090
091
                               121
      04
          04
                                      00
                                           Ü
                               122
123
      61 GTO
                                           Ū
                                      00
092
      33 X2
                                     00
                                           Ū
093
      76 LBL
                               124
                                     00
                                          O
094
      16 A'
                               125
                                     00
```

ANOVA TABLE

PROB-VALUE (2) F RATIO VARIANCE  $\frac{nS^2}{x}$ (C) DECREES OF FREEDOM (r - 1)(2)  $\begin{array}{ccc}
\mathbf{r} & \mathbf{r} \\
\mathbf{n} & \mathbf{\Sigma} & (\bar{\mathbf{x}}_{\mathbf{i}} - \bar{\mathbf{x}})^{2} \\
\mathbf{1} = \mathbf{1}
\end{array}$ SUM OF SQUARES SOURCE OF VARIATION BETWEEN ROWS

TOTAL  $\sum_{i} \sum_{j} (x_{i,j} - \bar{x})^2$  (nr - 1)

TABLE B-15

6

S22

 $\begin{array}{ccc}
\mathbf{r} & \mathbf{n} \\
\Sigma & \Sigma \\
\mathbf{i} & \mathbf{j} \\
\end{array} (\mathbf{x_{i,j}} - \bar{\mathbf{x}_{i,j}})^{2} & \mathbf{r(n-1)}$ 

WITHIN ROWS 9

(Z)

 $\bar{x}_{11}$ ٠۲̈ـ

 $\bar{x}_{\rm III}$ 

 $^{x}_{III5}$ 

~

SUBJECT

FITNESS EXAMPLE

I (Sedentary)

CATEGORY

 $^{\rm x}_{\rm I1}$ 

II (Runners)

 $x_{II3}$ 

III (Weightlifters)

 $\bar{\mathbf{x}}_{\mathbf{i}} = \frac{1}{n_{\mathbf{i}}} \sum_{\mathbf{i}, \mathbf{j}}$ 

n<sub>i</sub> = the number of subjects
 in Category i

 $\begin{array}{ccc} & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & \\ & & & \\ & &$ x = 1 r r

r = the number of categories

TABLE B-17

| Score     | 56.5                                   | 58                                     | 58                                     | 44.5                                   | 33.5                                   | 017                                    |
|-----------|--|--|--|--|--|--|
| 120 Sec   | 90                                     | 84<br>13                               | 78<br>14.5                             | 96                                     | 108                                    | 102<br>8.5                             |
| 90 Sec    | 90                                     | 90                                     | 90                                     | 102<br>8.5                             | 108                                    | 102                                    |
| 30 Sec    | 108                                    | 96<br>12                               | 102<br>10.5                            | 108                                    | 114                                    | 114                                    |
| Immediate | 114                                    | 114                                    | 126<br>8.5                             | 120<br>10                              | 132                                    | 126<br>8.5                             |
| Resting   | 66                                     | 72<br>10                               | 66                                     | 78                                     | 84                                     | 78                                     |
|           | Subject #1 - Heart Rate<br>Pipes Score | Subject #2 - Heart Rate<br>Pipes Score | Subject #3 - Heart Rate<br>Pipes Score | Subject #4 - Heart Rate<br>Pipes Score | Subject #5 - Heart Rate<br>Pipes Score | Subject #6 - Heart Rate<br>Pipes Score |

CATECORY I - CARDIOVASCULAR SCORES

# CATEGORY I - ADJUSTED STRENGTH SCORES

$$s_{11} = \frac{150 + 90}{190} = 1.26$$

$$s_{12} = \frac{130 + 75}{155} = 1.32$$

$$s_{13} = \frac{90 + 75}{170} = .97$$

$$s_{14} = \frac{160 + 85}{205} = 1.19$$

$$s_{15} = \frac{105 + 70}{157} = 1.13$$

$$s_{16} = \frac{110 + 75}{160} = 1.16$$

$$S_{1\bar{x}} = \frac{124 + 78}{173} = 1.17$$

#### CATEGORY I - ADJUSTED ENDURANCE SCORES

$$E_{11} = \left(\frac{100}{\text{BODY WT}}\right) \left(\frac{\text{NUMBER OF BENCH PRESS}}{\text{REPETITIONS}}\right) + \left(\frac{55}{\text{BODY WT}}\right) \left(\frac{\text{NUMBER OF CURL}}{\text{REPETITIONS}}\right)$$

$$E_{11} = (\frac{100}{190}) (31) + (\frac{55}{190}) (27) = 24.1$$

$$E_{12} = (\frac{100}{155}) (9) + (\frac{55}{155}) (20) = 12.9$$

$$E_{13} = (\frac{100}{170}) (0) + (\frac{55}{170}) (17) = 5.5$$

$$E_{14} = (\frac{100}{205}) (32) + (\frac{55}{205}) (46) = 27.9$$

$$E_{15} = (\frac{100}{157}) (2) + (\frac{55}{157}) (25) = 10.1$$

$$E_{16} = (\frac{100}{160}) (5) + (\frac{55}{160}) (23) = 11.0$$

$$E_{1\bar{x}} = (\frac{100}{173}) (13) + (\frac{55}{173}) (26) = 15.7$$

CATECORY II - CARDIOVASCULAR SCORES

|  | Resting    | Inmediate  | 30 Sec      | 60 Sec     | 120 Sec    | Score |
|--|------------|------------|-------------|------------|------------|-------|
| Subject #1 - Heart Rate<br>Pipes Score | 60<br>16   | 90<br>17.5 | 60<br>20    | 60         | 60<br>19   | 91.5  |
| Subject #2 - Heart Rate<br>Pipes Score | 48<br>19   | 90         | 60<br>20    | 748<br>70  | 448<br>20  | 5.96  |
| Subject #3 - Heart Rate<br>Pipes Score | 72<br>10   | 120<br>10  | 102<br>10.5 | 96<br>10   | 78<br>14.5 | 55.0  |
| Subject #4 - Heart Rate<br>Pipes Score | 54<br>17.5 | 90<br>17.5 | 66<br>19.5  | 60         | 54<br>20   | 93.5  |
| Subject #5 - Heart Rate<br>Pipes Score | 66<br>13   | 90<br>17.5 | 72<br>18    | 72<br>16   | 66<br>17.5 | 82    |
| Subject #6 - Heart Rate<br>Pipes Score | 60<br>16   | 108<br>13  | 72<br>18    | 66<br>17.5 | 66<br>17.5 | 82    |

TABLE B-20

## CATEGORY II - ADJUSTED STRENGTH SCORES

$$S_{21} = \frac{BENCH PRESS + CURL}{BOLY WEIGHT}$$

$$S_{21} = \frac{160 + 85}{167} = 1.47$$

$$S_{22} = \frac{170 + 105}{195} = 1.41$$

$$s_{23} = \frac{130 + 70}{180} = 1.11$$

$$S_{24} = \frac{150 + 80}{160} = 1.44$$

$$S_{25} = \frac{110 + 60}{127} = 1.34$$

$$s_{26} = \frac{100 + 75}{158} = 1.11$$

$$S_{2x} = \frac{137 + 79}{165} = 1.31$$

## CATEGORY II - ADJUSTED ENDURANCE SCORES

$$\mathbf{E_{21}} = (\frac{100}{\text{BODY WT}}) \; (\frac{\text{NUMBER OF BENCH PRESS}}{\text{REPETITIONS}}) \; + \\ (\frac{55}{\text{BODY WT}}) \; (\frac{\text{NUMBER OF CURL}}{\text{REPETITIONS}})$$

$$E_{21} = (\frac{100}{167}) (23) + (\frac{55}{167}) (25) = 22.0$$

$$E_{22} = (\frac{100}{195}) (31) + (\frac{55}{195}) (46) = 28.9$$

$$E_{23} = (\frac{100}{180}) (11) + (\frac{55}{180}) (20) = 12.2$$

$$E_{24} = (\frac{100}{160}) (14) + (\frac{55}{160}) (15) = 13.6$$

$$E_{25} = (\frac{100}{127})$$
 (5)  $+ (\frac{55}{127})$  (6)  $= 6.5$ 

$$E_{26} = (\frac{100}{158})$$
 (4) +  $(\frac{55}{158})$  (12) = 6.6

$$E_{2\bar{x}} = (\frac{100}{165}) (15) + (\frac{55}{165}) (21) = 16.1$$

CATECORY III - CARDIOVASCULAR SCORES

|  | Resting    | Immediate   | 30 Sec     | ce Sec     | 120 Sec     | Score |
|--|------------|-------------|------------|------------|-------------|-------|
| Subject #1 - Heart Rate<br>Pipes Score | 90         | 120<br>10   | 120<br>ć   | 102<br>8.5 | 108         | \$    |
| Subject #2 - Heart Rate<br>Pipes Score | % %        | 114         | 114 7.5    | 96<br>10   | 96<br>10    | 56.   |
| Subject #3 - Heart Rate<br>Pipes Score | 78         | 120<br>10   | 114        | 96<br>10   | 96          | 5.44  |
| Subject #4 - Heart Rate<br>Pipes Score | 54<br>17.5 | 90<br>17.5  | 44<br>15   | eë<br>17.5 | 60          | 86.5  |
| Subject #5 - Heart Rate<br>Pipes Score | 72<br>10   | 114<br>11.5 | 78<br>16.5 | 78<br>14.5 | 733<br>14.5 | 29    |
| Subject #6 - Heart Rate<br>Pipes Score | 844        | 138<br>5.5  | 132<br>3   | 120        | 108         | 24.5  |

TABLE B-23

## CATEGORY III - ADJUSTED STRENGTH SCORES

$$s_{3i} = \frac{BENCH PRESS + CURL}{BODY WEIGHT}$$

$$s_{31} = \frac{330 + 165}{200} = 2.48$$

$$s_{32} = \frac{320 + 155}{202} = 2.35$$

$$s_{33} = \frac{375 + 135}{205} = 2.49$$

$$s_{34} = \frac{305 + 185}{220} = 2.23$$

$$s_{35} = \frac{320 + 190}{180} = 2.83$$

$$s_{36} = \frac{320 + 130}{225} = 2.00$$

$$s_{3\bar{x}} = \frac{328 + 160}{205} = 2.38$$

# CATEGORY III - ADJUSTED ENDURANCE SCORES

$$E_{31} = (\frac{100}{BODY WT}) (\frac{NUMBER OF BENCH PRESS}{REPETITIONS}) + (\frac{55}{BODY WT}) (\frac{NUMBER OF CURL}{REPETITIONS})$$

$$E_{31} = (\frac{100}{200}) (67) + (\frac{55}{200}) (60) = 50.0$$

$$E_{32} = (\frac{100}{202}) (85) + (\frac{55}{202}) (75) = 62.5$$

$$E_{33} = (\frac{100}{205})(57) + (\frac{55}{205})(35) = 37.2$$

$$E_{34} = (\frac{100}{220}) (61) + (\frac{55}{220}) (60) = 42.7$$

$$E_{35} = (\frac{100}{180}) (70) + (\frac{55}{180}) (52) = 54.8$$

$$E_{36} = (\frac{100}{225})(54) + (\frac{55}{225})(31) = 31.6$$

$$\mathbb{E}_{3\bar{\mathbf{x}}} = (\frac{100}{205}) (66) + (\frac{55}{205}) (52) = 46.1$$

**TABLE B-26** 

| Subject #1 - Heart Rate |
|-------------------------|
| 19                      |
| 13                      |
| 60<br>16                |
| 66 13                   |
| 60<br>16                |
| 72<br>10                |

CATECORY IV - CARDIOVASCUIAR SCORES

# CATECORY IV - ADJUSTED STRENGTH SCORES

$$S_{4i} = \frac{BENCH \ PRESS + CURL}{BODY \ WEIGHT}$$
 $S_{4i} = \frac{290 + 170}{200} = 2.30$ 
 $S_{42} = \frac{305 + 175}{180} = 2.67$ 
 $S_{43} = \frac{205 + 125}{165} = 2.00$ 
 $S_{44} = \frac{230 + 120}{160} = 2.19$ 
 $S_{45} = \frac{310 + 135}{240} = 1.85$ 
 $S_{46} = \frac{275 + 155}{180} = 2.39$ 
 $S_{4\bar{x}} = \frac{270 + 147}{188} = 2.22$ 

# CATEGORY IV - ADJUSTED ENDURANCE SCORES

$$E_{\downarrow\downarrow 1} = (\frac{100}{\text{BODY WT}}) (\frac{\text{NUMBER OF BENCH FRESS}}{\text{REPETITIONS}}) + (\frac{55}{\text{BODY WT}}) (\frac{\text{NUMBER OF CURL}}{\text{REPETITIONS}})$$

$$E_{41} = (\frac{100}{200}) (52) + (\frac{55}{200}) (78) = 47.5$$

$$E_{42} = (\frac{100}{150}) (50) + (\frac{55}{180}) (64) = 49.0$$

$$E_{43} = \frac{100}{100}(44) + (\frac{55}{165})(51) = 43.7$$

$$E_{\downarrow\downarrow} = (\frac{100}{160}) (37) + (\frac{55}{160}) (70) = 47.2$$

$$E_{45} = (\frac{100}{240}) (55) + (\frac{55}{240}) (50) = 34.3$$

$$E_{46} = (\frac{100}{180}) (50) + (\frac{55}{180}) (55) = 44.6$$

$$E_{4\bar{x}} = (\frac{100}{188}) (49) + (\frac{55}{188}) (61) = 43.9$$

CATECORY V - CARDIOVASCUIAR SCORES

| sc Score  | 39.5                                   | 5 55                                   | 5 47                                   | 5 77.5                                 | 5 59.5                                 | 56.5                                   |
|-----------|--|--|--|--|--|--|
| 120 Sec   | 96                                     | 90                                     | 90                                     | 66<br>17.5                             | 78<br>14.5                             | 78                                     |
| 90 Sec    | 102<br>8.5                             | 90                                     | 90                                     | 72<br>16                               | 84<br>13                               | 90                                     |
| 30 Sec    | 108                                    | 102<br>10.5                            | 96                                     | 78<br>16.5                             | 102<br>10.5                            | 90                                     |
| Immediate | 132                                    | 114                                    | 126<br>8.5                             | 102<br>14.5                            | 126<br>8.5                             | 120<br>10                              |
| Resting   | 84                                     | 72<br>10                               | 90                                     | 66                                     | 66 13                                  | 78                                     |
|           | Subject #1 - Heart Rate<br>Pipes Score | Subject #2 - Heart Rete<br>Pipes Score | Subject #3 - Heart Rate<br>Pipes Score | Subject #4 - Heart Rate<br>Pipes Score | Subject #5 - Heart Rate<br>Pipes Score | Subject #6 - Heart Rate<br>Pipes Score |

# CATECORY V - ADJUSTED STRENGTH SCORES

$$S_{5i}$$
 =  $\frac{BENCH \ PRESS + CURL}{BODY \ WEIGHT}$ 
 $S_{51}$  =  $\frac{220 + 115}{165}$  = 2.03

 $S_{52}$  =  $\frac{265 + 160}{175}$  = 2.43

 $S_{53}$  =  $\frac{220 + 125}{185}$  = 1.86

 $S_{54}$  =  $\frac{200 + 110}{179}$  = 1.73

 $S_{55}$  =  $\frac{170 + 65}{205}$  = 1.15

 $S_{56}$  =  $\frac{140 + 70}{120}$  = 1.75

 $S_{5\bar{x}} = \frac{203 + 108}{172} = 1.81$ 

#### CATEGORY V - ADJUSTED ENDURANCE SCORES

$${\rm E}_{51} = (\frac{100}{\rm BODY~WT})~(^{\rm NUMBER~OF~BENCH~PRESS})~+ \\ (\frac{55}{\rm BODY~WT})~(^{\rm NUMBER~OF~CURL})$$

$$E_{51} = (\frac{100}{165}) (30) + (\frac{55}{165}) (22) = 25.5$$

$$E_{52} = (\frac{100}{175}) (37) + (\frac{55}{175}) (105) = 54.1$$

$$E_{53} = (\frac{100}{185}) (54) + (\frac{55}{185}) (60) = 47.0$$

$$E_{54} = (\frac{100}{179}) (33) + (\frac{55}{179}) (49) = 33.5$$

$$E_{55} = (\frac{100}{205}) (28) + (\frac{55}{205}) (31) = 22.0$$

$$E_{56} = (\frac{100}{120}) (22) + (\frac{55}{120}) (12) = 23.8$$

$$E_{5\bar{x}} = (\frac{100}{172}) (34) + (\frac{55}{172}) (47) = 34.8$$

TABLE B-32

|  | Resting        | Immediate   | 30 Sec     | 90 Sec     | 120 Sec    | Score |
|--|----------------|-------------|------------|------------|------------|-------|
| Subject #1 - Heart Rate<br>Pipes Score | 72<br>10       | 114<br>11.5 | 96         | 84<br>13   | 78<br>14.5 | 61    |
| Subject #2 - Heart Rate<br>Pipes Score | 78             | 126<br>8.5  | 108<br>9   | 90         | 90         | 47.5  |
| Subject #3 - Heart Rate<br>Pipes Score | 72<br>10       | 114         | 90<br>13.5 | 78<br>14.5 | 72<br>16   | 65.5  |
| Subject #4 - Heart Rate<br>Pipes Score | 60<br>16       | 102<br>14.5 | 72<br>18   | 66<br>17.5 | 60         | 85    |
| Subject #5 - Heart Rate<br>Pipes Score | 54<br>17.5     | .yo<br>17.5 | 78<br>16.5 | 66<br>17.5 | 66<br>17.5 | 86.5  |
| Subject #6 - Heart Rate<br>Pipes Score | 77<br>77<br>70 | 102<br>14.5 | 90         | 84<br>13   | 60         | 80    |

CATECORY VI - CARDIOVASCULAR SCORES

# CATEGORY VI - ADJUSTED STRENGTH SCORES

$$S_{61} = \frac{BENCH \ PRESS + CURL}{BODY \ WEIGHT}$$

$$S_{61} = \frac{155 + 100}{180} = 1.42$$

$$S_{62} = \frac{120 + 75}{125} = 1.56$$

$$S_{63} = \frac{130 + 85}{170} = 1.26$$

$$S_{64} = \frac{135 + 105}{170} = 1.41$$

$$S_{65} = \frac{145 + 90}{175} = 1.34$$

$$S_{66} = \frac{138 + 91}{171} = 1.34$$

## CATEGORY VI - ADJUSTED ENDURANCE SCORES

$$E_{61} = \left(\frac{100}{\text{BODY WT}}\right) \left(\frac{\text{NUMBER OF BENCH PRESS}}{\text{REPETITIONS}}\right) + \left(\frac{55}{\text{BODY WT}}\right) \left(\frac{\text{NUMBER OF CURL}}{\text{REPETITIONS}}\right)$$

$$E_{61} = (\frac{100}{180}) (25) + (\frac{55}{180}) (30) = 23.1$$

$$E_{62} = (\frac{100}{125}) (14) + (\frac{55}{125}) (14) = 17.4$$

$$E_{63} = (\frac{100}{170}) (14) + (\frac{55}{170}) (20) = 14.7$$

$$E_{64} = (\frac{100}{170}) (15) + (\frac{55}{170}) (20) = 15.3$$

$$E_{65} = (\frac{100}{175}) (10) + (\frac{55}{175}) (18) = 11.4$$

$$E_{66} = (\frac{100}{205}) (23) + (\frac{55}{205}) (25) = 17.9$$

$$E_{6\bar{x}} = (\frac{100}{171}) (17) + (\frac{55}{171}) (21) = 16.8$$

| ı×         |          | 7.87  | 83.4 | 52.2 | 83.4 | 55.8 | 6.02 |
|------------|----------|-------|------|------|------|------|------|
| 9#         |          | 0.04  | 82.0 | 24.5 | 71.5 | 56.5 | 80.0 |
| \$#        |          | 33.5  | 82.0 | 0.79 | 89.5 | 59.5 | 86.5 |
| 11#        |          | 144.5 | 93.5 | 86.5 | 79.0 | 77.5 | 85.0 |
| #3         |          | 58.0  | 55.0 | 0.44 | 85.0 | 0.74 | 65.5 |
| #5         |          | 58.0  | 96.5 | 96.0 | 0.67 | 55.0 | 47.5 |
| SUBJECT #1 |          | 56.5  | 91.5 | 95.0 | 5.96 | 39.5 | 61.0 |
|            | CALECORI | I     | ==   | 111  | 14   |      | ١٨   |

TABLE B-35

TABLE B-36

1.36 2.39 2.23 1.83 1.17 1.31 1× 1.15 2.00 2.39 1.75 1.16 1.11 9# 1.15 1.34 1.85 2.83 1.13 1.34 5# 2.19 1.73 1.41 2.23 1.191.44 **†**7# 1,26 2.00 1.86 2.49 1.11 % #3 1.56 2.67 2.43 2.35 1.41 1.32 #2 1.42 2.03 2.30 2.48 1.26 1.47 #1 SUBJECT CATECORY III٧I 17 Π

STRENCTH SCORES

| x 9#          |          | 11.0 15.25 | 6.6 14.96 | 31.6 46.46 | 44.38  | 23.8 34.32 | 17.9 16.63 |
|---------------|----------|------------|-----------|------------|--------|------------|------------|
| 45            |          | 10.1       | 6.5       | 54.8       | 34.3 4 | 22.0 2     | 11.4       |
| ##            |          | 27.9       | 13.6      | 42.7       | 47.2   | 33.5       | 15.3       |
| #3            |          | 5.5        | 12.2      | 37.2       | 43.7   | 0.54       | 14.7       |
| #5            |          | 12.9       | 28.9      | 62.5       | 0.64   | 54.1       | 17.4       |
| SUBJECT<br>#1 |          | 24.1       | 22.0      | 90.0       | 47.5   | 25.5       | 23.1       |
|               | CATECORY | 1          | II        | 111        | ΝĪ     | >          | ۷I         |

#### LIST OF REFERENCES

- 1. Army, Department of, Headquarters, FM 44-90, Washington, 1977.
- Army, Department of, Headquarters, Review of Selected Army Models, Washington, 1977.
- Astrand, Per-Olof and Rodahl, Kaare, <u>Textbook and Work Physiology</u>, Los Angeles: McGraw-Hill, 1978.
- 4. Barton, R. F., A Primer on Simulation and Gaming, p. 1-172, Prentice-Hall, 1970.
- 5. Braverman, J. D., Probability, Logic, and Management Decisions, p. 80-99, McGraw-Hill, 1972.
- 6. Kovach, L.D., Computer-Oriented Mathematics, p. 69-76, Holden-Day, 1964.
- 7. McCormick, Ernest, J., Human Factors in Engineering and Design, New York: McGraw-Hill, 1976.
- 8. Meredith, J. R. and Turban, E., Fundamentals of Management Science, p. 455-460, Business Publications, 1977.
- 9. Pipes, Thomas V., and Vodak, Paul A., The Pipes Fitness Test and Prescription, Los Angeles: J.P. Tarcher, 1978.
- 10. Texas Instruments, Programmable 58/59 Applied Statistics Library, 1977.
- 11. Texas Instruments, Programmable 58/59 Master Library, p. 52-54, 1977.
- 12. Texas Instruments, Personal Programming (A complete Owner's Manual for TI Programmable 58/59), 1977.
- 13. Wonnacott, R. J., and Wonnacott, T. H., <u>Introductory Statistics</u>, New York, John Wiley, 1977.
- 14. Zehna, P. W., Calculator Statistics: A TI 59 Supplement to Wonnacott and Wonnacott, Naval Postgraduate School, 1980.

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